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USER'S MANUAL FOR A FULLY AUTOMATIC THREE-DIMENSIONAL POTENTIAL--ETC(U)

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August 1, 1977

Report No. N67-214000

**USER'S MANUAL FOR A FULLY AUTOMATIC
THREE-DIMENSIONAL POTENTIAL FLOW CALCULATION METHOD**

**Part 2. With Viscous Correction
by Small Crossflow Boundary-Layer Analysis**

by

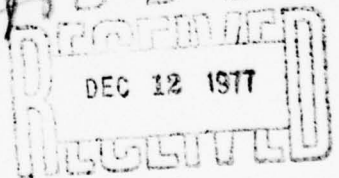
Dun-Pok Meek

This research was carried out under the Naval Ship
Systems Command General Hydrodynamics Research
Program Subproject SR 023 01 01, administered by the
Naval Ship Research and Development Center.

Contract N00014-74-C-0089

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**USER'S MANUAL FOR A FULLY AUTOMATIC
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POTENTIAL-FLOW CALCULATION METHOD

Part 2. With Viscous Correction by Small Crossflow
Boundary-Layer Analysis

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ABSTRACT .

This report describes a computer program which calculates three-dimensional viscous effects on the lift and pressure distributions of arbitrary three-dimensional bodies. The program is a combination of a panel method, which computes the potential flow about arbitrary three-dimensional lifting configurations, and a three-dimensional boundary-layer method, which calculates the viscous effects with small crossflow. These effects are applied to the three-dimensional shape, as in Part 1, in a "strip-theory" sense and the resultant viscous lift and pressure distributions are again produced. The method of simulating the boundary layer in the final potential-flow calculation is by the addition of the displacement thickness to the original shape.

The computer program is written in Fortran IV for the IBM 370 systems. 16 temporary external units are used for storage. The region size needed to execute the program is about 360K bytes, but this is a direct function of the number of elements defining the configuration.

Also presented in this report is a detailed description of the program logic, complete instructions for executing the program, and a sample case.

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1.0 INTRODUCTION

This is the second part of the user's manual for operating the combined three-dimensional potential-flow boundary-layer computer program. This part of the report concentrates on the procedure for obtaining the displacement thickness from the boundary-layer program in a three-dimensional form which allows for small crossflows.

The operation of this program is similar to that described in Part 1 [2]. The flow field data are generated and the input body shape is separated into lower and upper regions. The flow field data are then input to the streamline program to obtain the streamline curvature, orthogonal curvature and the streamline distances between the streamline points. These quantities are saved and reorganized to the form that is acceptable to the three-dimensional boundary-layer program which is based on that of reference 4.

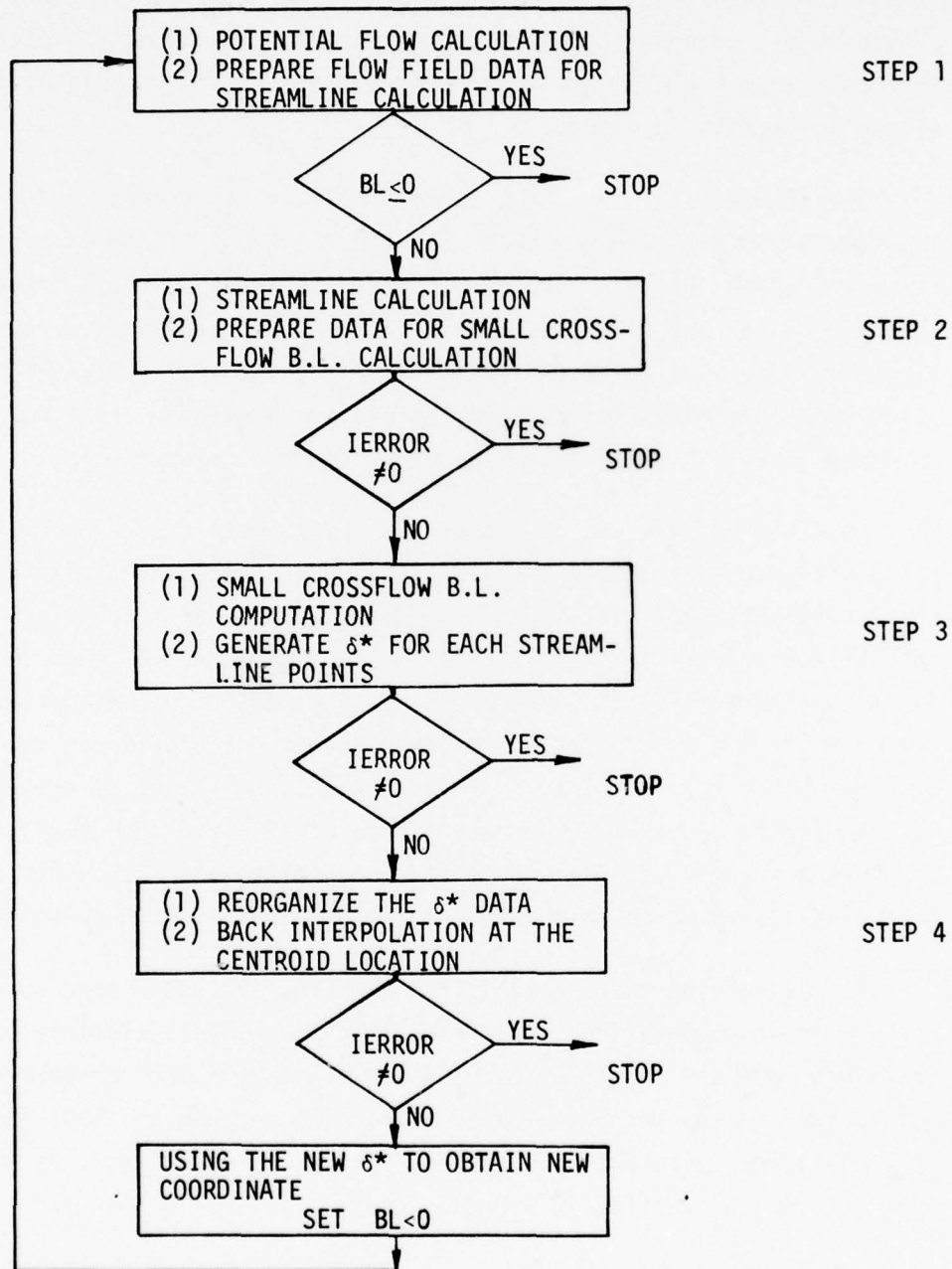
When the boundary-layer properties with small crossflows have been calculated, the displacement thicknesses, δ^* , associated with the streamline points are obtained. The lower and upper surface δ^* fields are defined at the streamline points. A surface interpolation method is used to obtain the δ^* at the control points that are used to compute the potential-flow calculation. After the interpolated δ^* procedure is accomplished, the surface displacement method of boundary-layer simulation is used as described in Part 1 of this manual. The generated coordinates are the coordinates with the boundary-layer effect. These new body points are once again input to the potential-flow program to obtain the final potential-flow solution.

At the present time, a multistep computer execution procedure is used for the above computation. This gives the user the flexibility to run the whole procedure as a single computer job, or to run each program step separately and examine the output at the end of each program step; in the latter case, data are saved and the user has the option of using it as input to the next step or to override it by card input.

All the programs should be compiled and stored before executing with data. The programs are written in Fortran IV language to be run in the IBM/370 system and a direct access unit is required in the streamline calculation.

2.0 PROGRAM NOTES

2.1 Program Logic Flow Diagram



2.2 Potential-Flow Calculation

The potential-flow calculation is performed initially to generate the flow-field data, i.e., the surface velocities, pressure coefficients, centroids and unit normals, etc. This calculation is used again after the displacement thickness has been added to the input body coordinates.

The major part of the potential-flow program is the same as described in Part 1 of this manual. There are a few additional routines here designed solely for the small crossflow version which are not needed in the version described in Part 1.

The functions of these particular routines are:

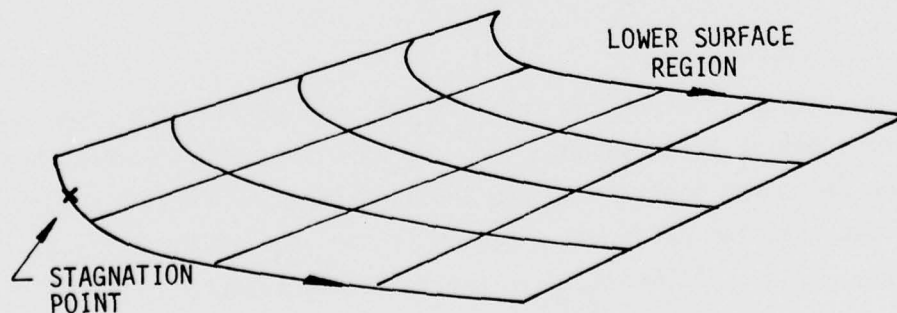
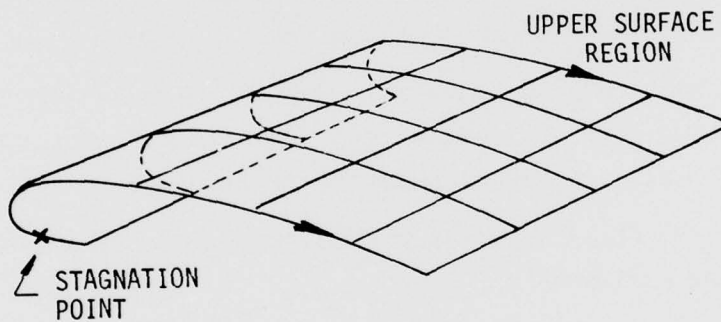
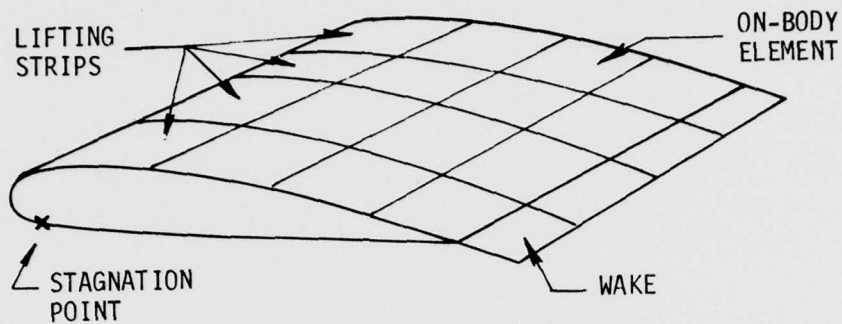
- (1) Compute the u, v coordinate of each input element and their derivatives with respect to x and y .
- (2) Compute the stagnation point and separate the input lifting body into two regions. Each region starts at three elements before the stagnation point and goes toward the trailing edge.
- (3) Organize the flow-field data of these regions to be used in the streamline routines.

The following units are saved:

- (1) Unit #2 — stores the u, v data.
- (2) Unit #21 — stores the flow-field data for each region.

2.3 Region Data Organization

A lifting section is separated into two regions; namely, the lower surface region and the upper surface region. Each region starts at a location near the stagnation point and goes toward the trailing edge. A lifting strip, therefore, is divided into two parts and a region is composed of the parts of these lifting strips. This is illustrated in the following sketch.



For each element in the region, there are 21 flow quantities associated with it, which over the whole region define the flow field that will be used for surface interpolation. The flow data and their storing sequence for each element follows.

(1) x_c	}	centroid component of the element.
(2) y_c		
(3) z_c		
(4) MU	}	equations (9) and (15) of [1].
(5) MV		
(6) V_ξ	}	velocities parallel to ξ and η axes. See 9.3 of [1].
(7) V_η		
(8) V_x	}	components of surface velocity
(9) V_y		
(10) V_z		
(11) U_o	}	nonorthogonal coordinates pertaining to the midpoint of a panel.
(12) V_o		
(13) a_{11}	}	components of the transformation matrix
(14) a_{12}		
(15) a_{13}		
(16) a_{21}		
(17) a_{22}		
(18) a_{23}		
(19) a_{31}		
(20) a_{32}		
(21) a_{33}		

These flow data are stored for each on-body element, strip by strip, from the starting element of the region to the trailing-edge element (excluding wakes). The lower surface is considered as region No. 1 and the upper surface is region No. 2. The program uses unit No. 21 to store the flow-field data. In addition to the flow-field data, eight quantities that are associated with the stagnation point for each strip are also stored following the flow-field data. They are:

(1) CPSTAG	pressure coefficient
(2) WESTAG	surface velocity
(3) XSTAG	} components of the stagnation point
(4) YSTAG	
(5) ZSTAG	

- | | | |
|---------|---|----------------------------------|
| (6) TSX | } | components of the tangent vector |
| (7) TSY | | |
| (8) TSZ | | |

The aforementioned data are all to be used in the streamline routine. Specifically there are three external units to be saved:

- (1) Unit #4 — geometry data of each element
- (2) Unit #2 — nonorthogonal coordinates
- (3) Unit #21 — flow-field data of the two regions

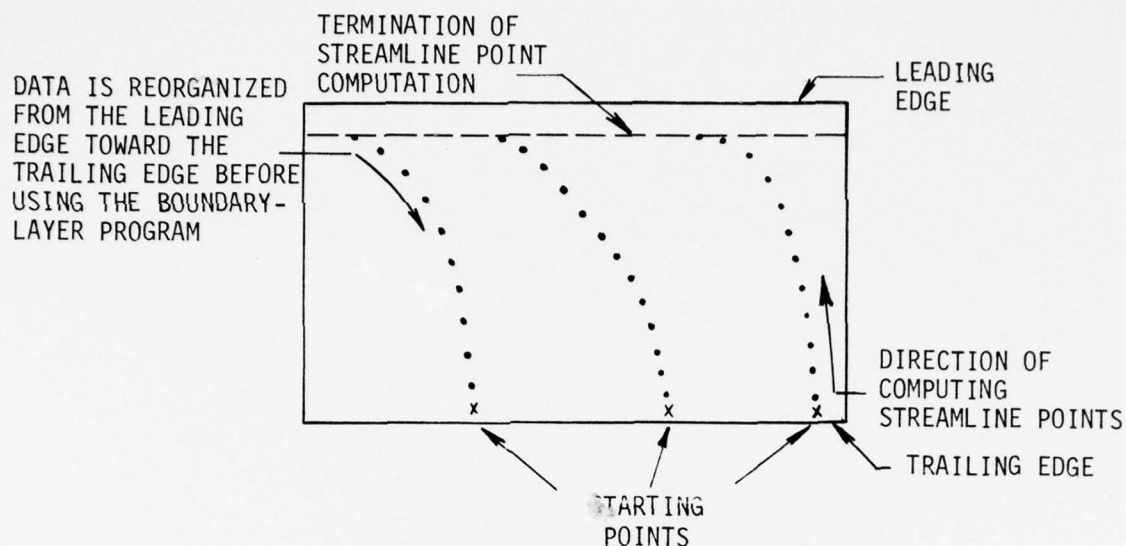
2.4 Streamline Calculation

The streamline calculation program is a modified version of the streamline calculation from the Mark IV supersonic-hypersonic arbitrary-body program [3]. A direct-access unit is used to store the flow-field data (the unit is defined as unit #10 in the program). Pointers for regions, and streamline points are saved so that users may use the same data again if the streamline program is to be run independently. The flow field data can be input by cards or passed from the potential-flow calculation program in unit #21 as stated previously.

After the flow-field data are input, an option is provided to check the flow-field data without going into the streamline calculation. If the streamline calculation is desired, the spacing between streamline points has to be input. The program will compute the streamline points from the trailing edge element toward the stagnation point using a fourth-order Runge-Kutta integration method with the user supplied spacing. Surface interpolation is performed to obtain the interpolated flow-field data at the streamline points. Orthogonal curvature is also computed at the same time.

Upon completion of all the streamline points for both regions, the program will organize the streamline data such that the order is from the stagnation point to the trailing edge. Streamline curvatures are also computed.

The following sketch illustrates the way the streamlines are calculated and organized for input to the boundary-layer calculation.



2.5 Boundary Layer with Small Crossflow Calculation

The small crossflow boundary-layer program used in this calculation is a modified version of [4]. The boundary-layer program uses the generated output from the streamline program, one streamline at a time, to compute the displacement thickness at each of the streamline points.

The input to this program requires the following data:

- (1) Number of points, station (x), the arc length between these stations, their curvature and their velocities.
- (2) Reynolds number per foot, reference velocity in ft/sec.
- (3) The point number of the transition location on each strip.

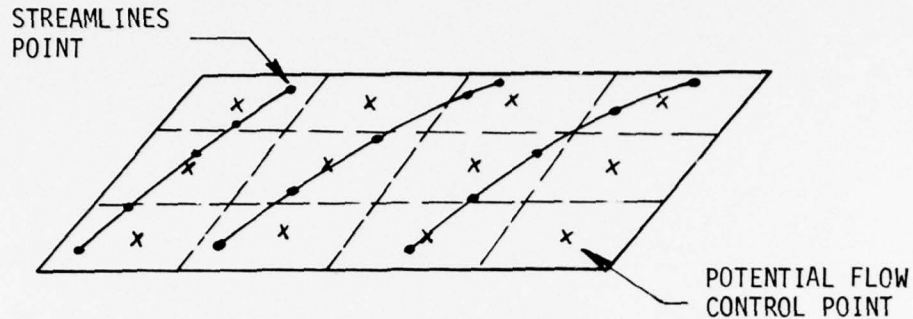
Items (1) and (2) above may be input by card as an option (see Section 3.3), as well as passed by the program. Only the transition location numbers must be input as punched cards.

On output, the displacement thicknesses (δ^*) are stored for each streamline point to be used for back interpolation.

2.6 Back Interpolation

The term back interpolation used here means that the displacement thickness values obtained from the small crossflow boundary-layer program at the streamline points, which define the δ^* over the whole region surface, are used to obtain δ^* at the original potential-flow calculation control points by using

the surface interpolation method as illustrated in the following figure.



After the δ^* at each control point is obtained, they are added to the original input coordinates in the same manner as described in Part I, [2] and in [1].

2.7 Simulation Program

This part of the program handles the generation of new coordinates with the δ^* added on as described in Part I [2]. Output may be saved on external units or punched on cards. They are used as input when recalling the potential-flow program.

2.8 Program Option

Listed below are the options that may be selected.

- (1) All of the potential-flow calculation options (note the restrictions mentioned in the next section).
- (2) Options to make a complete run in the streamline program or partial run to examine the data. Option to print every streamline point or every other point.
- (3) Option to input the flow-field data by cards or by external unit, i.e., tape or disk.
- (4) Print output option in the small crossflow boundary-layer program.

- (5) Option to execute the individual streamline in the small crossflow boundary-layer program.
- (6) Option to override the internally generated transition location.

2.9 Program Restriction

At present, this program is subject to the following restrictions:

- (1) Applicable only to the lifting body.
- (2) One angle of attack.
- (3) One section input.
- (4) The number of elements that define a region must not be greater than 500.
- (5) No more than 100 points per streamline.

3.0 INPUT INSTRUCTION

3.1 Potential Flow Program Input

Card 1 — Title card (required)

Format (18A4)

cc 1-68 TITLE Title of the case, 68 alphanumeric characters.

cc 69-72 TITLE(18) If two points (2 sets of x,y,z) per card input, leave blank.

If 1 point (1 set of x,y,z) per card input, punch "bØNE", where b means blank.

Card 2 — Control parameter card (required)

Format (A4, 13I3, 3F4.0, F12.0)

cc 1-4 CASE Case identification

cc 5-7 LIFSEC Total number of lifting sections

cc 8-10 MØMENT Moment origin input flag

cc 11-13 KUTTA Kutta point input flag

cc 14-16 NØFF Off-body point input flag

cc 17-19 LIST Partial execution flag

cc 20-22 MPR Matrix print flag

cc 23-25 IØUT Geometry quantities print flag

cc 26-28 IG Ignored element flag

cc 29-31 LASWAK Special last wake calculation flag

cc 32-34 IATAK Number of angles of attack

cc 35-37 IWIDTH Piecewise vorticity option flag

cc 38-40 ISAVE Stepwise pressure Kutta option

cc 41-43 IPCV Parabolic vorticity option flag

cc 44-47 SYM1 Flag for one plane symmetry

cc 48-51 SYM2 Flag for two planes of symmetry

cc 52-55 BL Flag for boundary-layer calculation

Note: For the calculation that this part of the report describes, the variables of this card should have the following values:

BL = 0 for final potential-flow calculation
after the new coordinates are generated.

cc 31-40	ALPHAX	} The x,y,z components of the second input angle of attack, if any. If there is no second input angle of attack, leave these fields blank.
cc 41-50	ALPHAY	
cc 51-60	ALPHAZ	

```
cc 1-10    ØRIGNX }
cc 11-20   ØRIGNY }   The x,y,z components of the input moment origin.
cc 21-30   ØRIGNZ }
```

```
cc 5-8      NWAKE(1)      Number of wake elements on each strip in the first
                        lifting section.
```

cc 9-12 NSTRIP(1) Number of strips in the first lifting section.

cc 13-16 IXFLAG(1) Extra strip flag in the first lifting section.

Note: The same format is repeated from cc 17-cc 64. Four lifting sections information can be put on 1 card and may repeat the same format on the next card if there are more than four sections. Users are advised to use only 1 lifting section if streamline calculation is used.

Card 6 – Ignored Element Card (optional)

Format (16I4)

cc 1-4 IG1(1,1) First element number on the first strip of the first lifting section to be ignored.

cc 5-8 IGN(1,1) Last element number on the first strip of the first lifting section to be ignored.

Note: This card is needed only if IG≠0 on card 2. Repeat the same format for the other strips of the same section. Start a new card for another section.

Card 7 – Strip widths card (required)

Format (6E10.0)

cc 1-10 WIDXTR Width of the first extra strip of the first section, if any. If no extra strip input, leave blank.

cc 11-20 WIDTH(1,1) Width of the first strip of the first lifting section.

cc 21-30 WIDTH(2,1) Width of the second strip of the first lifting section.

cc 31-40 WIDTH(3,1) Width of the third strip of the first lifting section.

Note: Repeat the same format with 6 strip widths per card. After the last strip width, it should follow by the strip width of the last extra strip of the section whether there is extra strip input or not. 0.0 is used if there is no input last extra strip.

Card 8 – Body definition card (required)

Format (2(3E10.0,2I1) – For 2 input points per card

Format (3E10.0, 2I1) – For 1 input point per card

cc 1-10	X	}	x,y,z components of the input point.
cc 11-20	Y		
cc 21-30	Z		

cc 31	STATUS	Status flag
		0 = same n-line
		1 = new n-line
		2 = new section
		3 = end input

cc 32	LABEL	Element type
		0 = nonlifting
		1 = lifting

Note: Repeat the same group from cc 33 - cc 64 for the next input point, if two points per card format were used.

Card 9 - Kutta control point card (optional)

Format (6E10.0)

cc 1-10	CUTTAX(I)	}	x,y,z components of the first input Kutta control points.
cc 11-20	CUTTAY(I)		
cc 21-30	CUTTAZ(I)		

cc 31-40	CUTTAX(I+1)	}	x,y,z components of the next input Kutta control points.
cc 41-50	CUTTAY(I+1)		
cc 51-60	CUTTAZ(I+1)		

Note: This card is used only when KUTTA#0 on card 2.

Card 10 - Kutta normal card (optional)

Format (6E10.0)

cc 1-10	CNX(I)	}	x,y,z components of the input Kutta control point normal vector.
cc 11-20	CNY(I)		
cc 21-30	CNZ(I)		

cc 31-40	CNX(I+1)	}	x,y,z components of the next input Kutta control point normal vector.
cc 41-50	CNY(I+1)		
cc 51-60	CNZ(I+1)		

Note: This card is needed only if KUTTA#0 on card 2.

Card 11 - Off-body point card (optional)

Format (2(3E10.0,I1))

cc 1-10	XOFF(I)	}	x,y,z components of the input off-body points.
cc 11-20	YOFF(I)		
cc 21-30	ZOFF(I)		

cc 31	LABEL	Status flag
-------	-------	-------------

cc 32-41	XOFF(I+1)	} x,y,z components of the next off-body point.
cc 42-51	YOFF(I+1)	
cc 52-61	ZOFF(I+1)	

cc 62 LABL Status flag

Note: LABL=3 at the end of the off-body point input, otherwise leave it blank. This card is needed only when NOFF≠0.

2.4 Flow Program Input

 - title and option card (required)

Format (18A4,I2)

cc 1-72 TITLE Any appropriate title for the case to be run.

cc 73-74 IOPT Option flag
 IOPT=0 No option used.
 IOPT=1 No streamline calculation but uses the previous streamline results to prepare for the small crossflow boundary-layer calculation.
 IOPT=2 Streamline calculation only.

Note: When the flow-field data of the case is loaded first time onto the direct-access unit, set TITLE(18)="bbb1" this enables the program to print the data for user to check.

Card 2 - Master directory title card (required)

Format (1I1,19X,10A4)

cc 1 MFLAG MFLAG=0 to initialize the master directory, i.e., anytime user wishes to override the direct-access data or defines a new data file.
 MFLAG≠0 Implies the data set has been previously stored.

cc 21-60 TITLEM Any description for the master directory.

Card 3 - Set directory title card (required)

Format (2I1,1X,I1,F6.0,10X,10A4)

cc 1 LASTS This flag should be set = 1.

cc 2 NEWS NEWS=0 New data set input.
 NEWS≠0 Data set already stored.

cc 4 NSET Data set number. This should be set = 1.

cc 5-10 MACH Mach number

cc 21-60 TITLES Any description of the set title.

Card 4 - Region set control card (required)

Format (2I1,I2,2F6.0,4X,10A4)

cc 1	LASTAB	LASTAB=0	Indicates more than one region.
		LASTAB \neq 0	Means this is the last region.
cc 2	NEWAB	NEWAB=0	For new region.
		NEWAB \neq 0	For subsequent regions.
cc 3-4	IAB	Region number	
cc 5-10	ALPHA	α value	These values should be set =0 when input.
cc 11-16	BETA	β value	
cc 21-60	TITLEA	Region title	

Note: Lower surface of the wing is considered as Region #1, and upper surface is considered as Region #2 in this program.

Card 5 - Subregion set control card (required)

Format (2I1,I2,3I1,13X,10A4)

cc 1	LASTR	LASTR=0	Indicates more than 1 subregion within the region.
		LASTR \neq 0	Implies this is the last subregion.
cc 2	NEWR	NEWR=0	For new subregion.
		NEWR \neq 0	For subsequent subregions within the region data set.
cc 3-4	IREG	Subregion set number.	
cc 5	IDTYP(1)	This field is always set equal to 2 .	
cc 6	ISORCE	This field is not used at present and is set to 0.	
cc 7	IRW	Data read or write flag	
		IRW=0	Data will be input and saved on direct-access unit 10.
		IRW=1	Data has been saved and will be read in from direct-access unit 10.
cc 21-60	TITLER	Subregion title	

Note: Cards numbered 4, 5 used as a group for the lower surface of a wing. The same group of cards is used for the upper surface before the next card is input.

Card 6 - Streamline input card #1 (required)

Format (I1,3I2,3I1,10I2,5I1,3F10.7)

cc 1	LASTR	Last flow region flag LASTR=0 This is not the last streamline set of data. After all the streamlines for this region are calculated, subroutine STREAM will read another region data from unit 10 and input. LASTR=1 This is the last region. After the streamline for this region is completed, no further region data will be read.
cc 2-3	NDSET	Data set number where surface flow data will be found on #10. Note: This flag should be the same as NSET on card 3.
cc 4-5	IABSET	Region set number. This number should be agreeable to IAB in card 4.
cc 6-7	IR	Subregion number. This number should be the same as IREG on card 5.
cc 8	INORM	This field is set equal to 0.
cc 9	ISURF	This field is set equal to 0.
cc 10	IPF	This field is set equal to 0.
cc 11-30	ISR(1) } to ISR(10) }	Subregion flow number. Since this version of the program does not use subregion, ISR(1)=1, and the rest of the array is set equal to 0.
cc 31-35	ISF(1) } to ISF(5) }	Secondary flow number. The whole array is set equal to 0.
cc 36-45	DELTA1	A criteria used with EPS1 to ensure that the streamline point has reached the stagnation line. Suggested value = 0.999.
cc 46-55	EPS1	Suggested value for this criteria is 0.01.
cc 56-65	EPS2	A criteria for terminating the streamline calculation, if the difference between two successive coordinates is less than EPS2. Suggested value 0.001.

Card 7 — Streamline input card #2 (required)

Format (2I2,16X,10A4)

cc 1-2	IRSAVE	Streamline save flag IRSAVE=0 Do not save. IRSAVE#0 Streamline data will be saved on unit 10.
cc 3-4	NSTR	Number of streamlines to be calculated for the input region number.
cc 21-60	TITLER	Title for streamline flow region.

Card 8 — Streamline input card #3 (required)

Format (2I2,3I1,I2,I4,7X,4F10.0)

cc 1-2	IPRINT	Streamline print flag. IPRINT=0 No streamline data will be printed. IPRINT=2 Print streamline data for every second DELTAS point. IPRINT=3 Print streamline data for every third DELTAS point. etc.
cc 3-4	ISAVE	Streamline save flag. ISAVE=0 No streamline data will be used. ISAVE=2 Save streamline data for every second DELTAS point. ISAVE=3 Save streamline data for every third point. etc.
cc 5	ISTART	Streamline starting condition flag. ISTART=1 Starting point of streamline. Calcula- tion is obtained from unit #10. ISTART#1 User will input the starting point of the streamline calculation.
cc 6	ISTAG	} These fields should be left blank at present.
cc 7	ISMØDE	
cc 8-9	IPANL	
cc 10-13	L	
cc 21-30	DELTAS	Streamline integration distance step interval for the Runge-Kutta integration process. (May be negative to integrate forward.)
cc 31-40	XSI	} x,y,z components of the streamline starting point. Input these fields only if ISTART#1.
cc 41-50	YSI	
cc 51-60	ZSI	

Repeat card no. 9 as many times as the number of streamline NSTR input in card no. 8.

Note: Cards nos. 7, 8, 9 are input as a group for one region (say, lower surface of the wing). If LASTR=0 is input in card no. 7, then the same cards (i.e., 7, 8, 9) should be used again for additional region.

Card 9 — Reference velocity and Reynolds number card (required)

Format (3F15.6)

cc 1	VREF	Reference velocity in ft/sec to be used in boundary-layer program.
cc 16	REREF	Reynolds number in unit of ft^{-1} .
cc 31	SF	Input scale factor to convert the basic points in the unit of ft. For example, if the original input to the potential-flow program is in inches, then the SF here should be input as 12 so the program can convert the points to feet. SF is input as 1.0 if original input is already in feet.

3.3 Small Crossflow Boundary-Layer Program Input

Card 1 — Option card (required)

Format (6I5)

cc 1-5	NCASE	Total number of cases input. Example: If there are six streamlines in one region (say, lower surface), then NCASE=6, etc.
cc 6-10	INTAPE	Unit number that contains the input data.
cc 11-15	IOUTAP	Unit number that will contain the output.
cc 16-20	IØPT	Print option flag. IØPT=0 Short print IØPT=1 Selected output print IØPT=2 Long print
cc 21-25	JØPT	Selects input region number and streamline number to be executed. This option is designed for users who wish to execute only the selected streamlines in the boundary-layer program and skip the rest of the streamlines. JØPT=0 Execute every streamline. JØPT≠0 Input the region number and streamline number. Notice that if only 3 streamlines were selected, then NCASE=3 is in cc 5.

cc 26-30	NØPT	NØPT=0	Program will use the input transition location.
		NØPT≠0	Program will check the input transition location. If the input transition location is beyond the acceptable range, the program will override it with a location that coincides with the change of velocity profile.

Card 2 – Region and streamline number input card (optional)

Format (20A4)

cc 1-4	SET(1)	Region number in which the streamline will be used.
cc 5-8	SLINE(1)	Streamline number to be executed in the boundary-layer program.

Repeat the same format for the next selected streamline to be executed. The streamline numbers may be entered on one card. This card is not needed if JØPT=0 is entered on card 1.

Card 3 – Region title card (optional)

Format (16A4)

cc 1-40	TITLE(1) to TITLE(10)	} Any suitable header.
cc 41-44	TITLE(11)	
cc 60-64	TITLE(16)	This field should contain streamline number.

Note: If the data come from a prestored unit, i.e. INTAPE#5, this card is not required.

Card 4 – Control flag card (optional)

Format (5I1,3I3,3E14.6)

cc 1	FL1	This flag is set equal to 1.
cc 2	FL2	This flag is set equal to 2.
cc 3	FL3	} These flags are set equal to 0.
cc 4	FL4	
cc 5	FL5	
cc 6-8	NXT	Total number of points.
cc 9-11	NTR	Transition location.

cc 12-14	NNN	(Not used)
cc 15-28	VGP	VGP=1.14
cc 29-42	DETA1	DETA1=0.01
cc 43-56	EPS	EPS=0.001

Note: This card is needed only if INTAPE=5.

Card 5 — Velocity and Reynolds number card (optional)

Format (4E14.6)

cc 1-14	VREF	Reference velocity in ft/sec.
cc 15-28	REREF	Reynolds number in ft^{-1}
cc 29-42	SWANG	This field is input with 0.0
cc 43-56	P30	P30=1.0 for user input.

Note: This card is required only if INTAPE=5.

Card 6 — Station data card (optional)

Format (4E14.6)

cc 1-14	X(I)	Streamline distance between point I and the starting point.
cc 15-28	UE(I)	Surface velocity at Ith station.
cc 29-42	RK1(I)	Orthogonal curvature at Ith station.
cc 43-56	RK2(I)	Streamline curvature at Ith station.

Note: One station data per card. Repeat the same format for another station. This card is needed only if INTAPE=5.

Card 7 — Transition location card (required)

Format (I5)

cc 1-5	NTR	Streamline point number designated as the user input transition location. Note that point No. 1 is the stagnation point.
--------	-----	--

4 Back Interpolation Program Input

Card 1 — Data set title card (required)

Format (16A4,I4)

cc 1-64	TITLE	Header of the region to be executed.
---------	-------	--------------------------------------

cc 65-68 ISET ISET=1 For one region.
 ISET=2 For two regions.

Card 2 — External unit definition card (required)

Format (14I5)

cc 1-5	IØUTAP	Unit number from boundary-layer program which stores the δ^* values.
cc 6-10	IUNITB	Scratch units to be used in the matrix solution subroutines.
cc 11-15	IUNITC	
cc 16-20	IUNITD	
cc 21-25	IFT20	Unit number from the potential-flow program which stores the U_0, V_0 values. This unit number is defined as no. 20. User may change it in the potential-flow program if so desired.
cc 26-30	IFT22	Unit number that stores the interpolated δ^* at the potential-flow calculation control points. This is the output unit from this program and it will be used in the final potential-flow computation.
cc 31-35	KSØRCE	Number of source elements per lifting strip as input to the potential-flow program.
cc 36-40	KWAKE	Number of wake elements per lifting strip as input to the potential-flow program.
cc 41-45	IEXTRA	Number of extra strips as input to the potential flow program.

Card 3 — Streamline information card (optional)

Format (14I5)

cc 1-5	ISTRM(I)	Streamline region number.
cc 6-10	NSLINE(I)	Number of streamlines within the region.
cc 11-15	LSTART(I)	Starting address of the first streamline within the region.
cc 16-20	ILIM1(I)	Starting element number of the strip from potential-flow program that is used as the lower limit of the region.
cc 21-25	ILIM2(I)	Ending element number of the strip from the potential-flow program that is used as the upper limit of the region.

Note: This card is needed only if user wants to run this program as a separate run. Otherwise data will be stored and passed into this program.

Card 4 — u,v data card (optional)

Format (6F12.6)

cc 1-12	UTE(I)	u-coordinate of the u-v plane at the trailing edge. This is calculated in the potential-flow program.
cc 13-24	ULE(I)	u-coordinate at the leading edge. Obtained from potential-flow program.
cc 25-36	VTE(I)	v-coordinate of the u-v plane at the trailing edge. This is calculated in the potential-flow program.
cc 37-48	VLE(I)	v-coordinate at the leading edge.
cc 49-60	CRØØT(I)	Distance of the root chord in the u-v plane between the trailing edge and the leading edge. This is obtained from streamline program.
cc 61-72	CTIP(I)	Distance of the tip chord in the u-v plane between the trailing edge and the leading edge. This also is obtained from streamline program.

Note: All the above data is for region I. This card is needed only if the program is run separately.

Card 5 — Streamline output condition card (optional)

Format (14I5)

cc 1-5	NSPT(I,IS)	Number of streamline points of the Ith streamline in the ISth region.
cc 6-10	ICØND(I,IS)	ICØND=0 Means the streamline computation ends normally and the points can be used. ICØND=1 Indicates the streamline computation does not end normally and this streamline should be skipped. I For streamline count. IS For region number.
cc 11-15	LPØINT(I,IS)	Starting address in the direct-access unit #10 to be used for retrieving the streamline data.

Note: One streamline information per card. Repeat the same format for another streamline. This card is needed only if the program is run independently.

3.5 Final Potential-Flow Program Computation

This part of input is the same as the initial potential-flow program (see 3.1) with the following exceptions:

1. BL on card 2 is input with a negative value, say -1.0.
2. Body points input is not needed.

The remaining input is the same as the initial potential-flow calculation input.

4.0 DECK SETUP

Two types of JCL deck setups are given for a multistep job. The first type shows the JCL setup for computing, linked editing and executing each step of the program. The second JCL setup is for the case where all the steps of the program have been stored on a diskpack prior to execution.

Although these examples are for a multistep job, each program may be run individually. In this case, the data sets to be saved in each step should be kept rather than passed into the next program step. For example, in the potential-flow program, initial calculations, there is a DD-card for Unit 21 defined as follows:

```
//GO.FT21F001 DD DSN=RUNCASE.FLOWDATA,UNIT=TAPE16,  
//           DISP=(NEW,PASS),  
//           DCP=(RECFM=VBS,BLKSIZE=6447,BUFNØ=1),  
//           LABEL=(1,SL,RETPD=180)
```

The disposition parameter indicates that this data set is to be passed into the next step, i.e., the streamline calculation program. However, if it is desired to save this data set and use it at a later time, this can be accomplished by changing the disposition parameter to:

```
DISP=(NEW,KEEP),
```

in the aforementioned DD-card.

It is also possible to allow a certain data set to be punched on cards rather than saved on tape or disk. In that case, the punch cards may be input to the next program after the output of the previous program has been examined. This capability is applicable to those data sets that have the record format RECFM=FB defined in the DD statement.

In short, if these program steps are to be run independently, it is necessary to change some JCL parameters. Users may have to alter the JCL decks according to the system they are using.

4.1 JCL Setup for Compiling the Source Program, Linkediting the Compiled Module and Running Data

(a) Potential Flow Program, Initial Calculation

Card Columns

0 1 2 3 4 5 6 7
1234567890123456789012345678901234567890123456789012

```
//STEP1 EXEC FORTXCLG,PARM.FORT='XREF,OPT=2',
//          PARM.LKED='MAP,LIST,OVLV',REGION.GD=380K
//FORT.SYSUT2 DD DSN=&SYSUT2,UNIT=SYSDA,SPACE=(TRK,(5,5))
//FORT.SYSIN DD *
//          ( REPLACE THIS CARD WITH POTENTIAL FLOW PROGRAM DECKS. )
/*
//LKED.SYSIN DD *
  ENTRY MAIN
  OVERLAY ALPHA
    INSERT BDFORM
    INSERT POINTS
    INSERT MISC
    INSERT NOLIFT
    INSERT LIFT
  OVERLAY BETA
    INSERT INPUT
  OVERLAY BETA
    INSERT DINPUT
  OVERLAY ALPHA
    INSERT UVGEN
  OVERLAY ALPHA
    INSERT VFORM
    INSERT MOMENT
    INSERT FIELDS
  OVERLAY BETA
    INSERT VMNLF
  OVERLAY BETA
    INSERT VFMLFT
  OVERLAY ALPHA
    INSERT PSWISE
  OVERLAY ALPHA
    INSERT AFORM
  OVERLAY ALPHA
    INSERT MATSOL
    INSERT SPACER
  OVERLAY BETA
    INSERT COLSOL
  OVERLAY BETA
    INSERT SOLMOR
  OVERLAY ALPHA
    INSERT COMFLO
    INSERT MISI
    INSERT FINAL
  OVERLAY BETA
    INSERT PKUTTA
  OVERLAY BETA
    INSERT PRINT
  OVERLAY ALPHA
    INSERT GETRDY
  OVERLAY ALPHA
    INSERT MODXYZ
```

(continued)

Card Columns

0	1	2	3	4	5	6	7
12345678901	2345678901	2345678901	2345678901	2345678901	2345678901	2345678901	23456789012
//GO.FT01F001	DD	DSNAME=&FT01,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT02F001	DD	DSN=RUNCASE,UVDATA,	UNIT=TAPE16,	DISP=(NEW,PASS),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1),			
//		LABEL=(1,SL,	RETPD=180)				
//GO.FT03F001	DD	DSNAME=&FT03,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT04F001	DD	DSN=RUNCASE,GEOMDATA,	UNIT=TAPE16,	DISP=(NEW,PASS),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1),			
//		LABEL=(1,SL,	RETPD=180)				
//GO.FT07F001	DD	SYSOUT=B					
//GO.FT08F001	DD	DSNAME=&FT08,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT09F001	DD	DSNAME=&FT09,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT10F001	DD	DSNAME=&FT10,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT11F001	DD	DSNAME=&FT11,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT12F001	DD	DSNAME=&FT12,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT13F001	DD	DSNAME=&FT13,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT14F001	DD	DSNAME=&FT14,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT15F001	DD	DSNAME=&FT15,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT16F001	DD	DSNAME=&FT16,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT17F001	DD	DSNAME=&FT17,	UNIT=SYSDA,	SPACE=(TRK,(10,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT18F001	DD	DSNAME=&FT18,	UNIT=SYSDA,	SPACE=(TRK,(10,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT19F001	DD	DSNAME=&FT19,	UNIT=SYSDA,	SPACE=(TRK,(10,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT21F001	DD	DSN=RUNCASE,FLOWDATA,	UNIT=TAPE16,	DISP=(NEW,PASS),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1),			
//		LABEL=(1,SL,	RETPD=180)				
//GO.FT23F001	DD	DSN=&FT23,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.FT24F001	DD	DSN=&FT24,	UNIT=SYSDA,	SPACE=(TRK,(50,5)),			
//		DCB=(RECFM=VBS,	BLKSIZE=6447,	BUFNO=1)			
//GO.SYSIN DD *							
/*		(REPLACE THIS CARD WITH THE INPUT DATA TO POTENTIAL FLOW PROG.)					

(b) The Streamline Calculation Program

Card Columns

0 1 2 3 4 5 6 7
1234567890123456789012345678901234567890123456789012

```
//STEP2 EXEC FORTXCLG,PARM.FORT='OPT=2,XREF',REGION.GC=250K
//FORT.SYSUT2 DD DSN=&SYSUT2,UNIT=SYSDA,SPACE=(TRK,(5,5))
//FORT.SYSIN DD *
  ( REPLACE THIS CARD WITH THE STREAMLINE CALCULATION PROGRAM DECKS. )
/*
//GO.FT01F001 DD DSN=OUTDATA.TL4FY,UNIT=TAPE16,DISP=(NEW,PASS),
//              DCB=(RECFM=FB,LRECL=80,BLKSIZE=4000),
//              LABEL=(1,SI,RETPD=190)
//GO.FT02F001 DD DSN=&FT02,UNIT=SYSDA,SPACE=(TRK,(50,10)),
//              DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT03F001 DD DSN=&FT03,UNIT=SYSDA,SPACE=(TRK,(50,10)),
//              DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT04F001 DD DSN=&FT04,UNIT=SYSDA,SPACE=(TRK,(50,10)),
//              DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT07F001 DD SYSOUT=B
//GO.FT10F001 DD DSN=DAC.EOH3.DPM.J14B.RUNCASE,UNIT=3330-1,
//              DCB=(DSORG=QA,BUFNO=1),VOL=SER=CSLB30,DISP=(NEW,PASS)
//              SPACE=(100,(2000))
//GO.FT15F001 DD DSN=*.STEP1.GO.FT02F001,DISP=(OLD,PASS)
//GO.FT16F001 DD DSN=*.STEP1.GO.FT04F001,DISP=(OLD,PASS)
//GO.FT21F001 DD DSN=*.STEP1.GO.FT21F001,DISP=(OLD,KEEP)
//GO.SYSIN DD *
  ( REPLACE THIS CARD WITH THE INPUT DATA TO THE STREAMLINE PROG. )
/*
```

(c) The Small Crossflow Boundary-Layer Program

Card Columns

0 1 2 3 4 5 6 7
1234567890123456789012345678901234567890123456789012

```
//STEP3 EXEC FORTXCLG,PARM.FORT='XREF,OPT=2',REGION.GO=200K
//FORT.SYSUT2 DD DSN=&SYSUT2,UNIT=SYSDA,SPACE=(TRK,(5,5))
//FORT.SYSIN DD *
( REPLACE THIS CARD WITH THE BOUNDARY LAYER PROGRAM DECK. )
/*
//GO.FT01F001 DD DSN=*.STEP2.GO.FT01F001,DISP=(OLD,KEEP)
//GO.FT02F001 DD DSN=DSTAR.FL4FY,UNIT=TAPE16,DISP=(NEW,PASS),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=4000),
// LABEL=(1,SL,RETPD=180)
//GO.FT03F001 DD DSN=*.STEP1.GO.FT02F001,DISP=(OLD,PASS)
//GO.FT04F001 DD DSN=*.STEP1.GO.FT04F001,DISP=(OLD,PASS)
//GO.FT10F001 DD DSN=*.STEP2.GO.FT10F001,DISP=(OLD,PASS)
//GO.FT07F001 DD SYSOUT=B
//GO.SYSIN DD *
( REPLACE THIS CARD WITH THE INPUT DATA TO THE BOUNDARY LAYER PROG )
/*
```

(d) The Back Interpolation Program

```
//STEP4 EXEC FORTXCLG,PARM.FORT='XREF,OPT=2',REGION.GO=220K
//FORT.SYSUT2 DD DSN=&SYSUT2,UNIT=SYSDA,SPACE=(TRK,(5,5))
//FORT.SYSIN DD *
( REPLACE THIS CARD WITH THE BACK INTERPOLATION PROGRAM DECKS. )
/*
//GO.FT01F001 DD DSN=*.STEP3.GO.FT02F001,DISP=(OLD,KEEP)
//GO.FT02F001 DD DSN=&FT02,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT03F001 DD DSN=&FT03,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT04F001 DD DSN=&FT04,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT07F001 DD SYSOUT=B
//GO.FT10F001 DD DSN=DAC.F0H3.DPM.J1HB.RUNCASE,UNIT=3330-1,
// DCB=(DSORG=DA,BUFNO=1),VOL=SER=CSLB30,DISP=(OLD,KEEP),
// SPACE=(100,(2000))
//GO.FT16F001 DD DSN=*.STEP1.GO.FT04F001,DISP=(OLD,PASS)
//GO.FT20F001 DD DSN=*.STEP1.GO.FT02F001,DISP=(OLD,KEEP)
//GO.FT22F001 DD DSN=DSTAR.TJ1HB,UNIT=TAPE16,DISP=(NEW,PASS),
// DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1),
// LABEL=(1,SL,RETPD=180)
//GO.SYSIN DD *
( REPLACE THIS CARD WITH THE INPUT DATA TO THE BACK INTERP. PROG. )
/*
```

(e) The Final Calculation Using the Potential Flow Program.

Note that the potential-flow program is assumed to be stored on a volume identified as "CSLB30" with the data set name "DAC.EOH3.DPM.J1HB.V3".

0 1 2 3 4 5 6 7
12345678901234567890123456789012345678901234567890123456789012

```

//STEP5 EXEC FORTORTIO,REGION=380K
//STEPL1R DD DSN=DAC.EQH3.DPM.J1HB.V3,DISP=(SHR,PASS),UNIT=3330-1,
// VOL=SER=CSLB30
//
//GC.SYSIN DD *
//GC.FT01F001 DD DSN=&FT01,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GC.FT02F001 DD DSN=&FT02,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT03F001 DD DSN=&FT03,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT04F001 DD DSN=&FT04,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT07F001 DD SYSDA=8
//GC.FT08F001 DD DSN=&FT08,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT09F001 DD DSN=&FT09,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT10F001 DD DSN=&FT10,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT11F001 DD DSN=&FT11,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT12F001 DD DSN=&FT12,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT13F001 DD DSN=&FT13,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT14F001 DD DSN=&FT14,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT15F001 DD DSN=&FT15,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT16F001 DD DSN=&FT16,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT17F001 DD DSN=&FT17,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT18F001 DD DSN=&FT18,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT19F001 DD DSN=&FT19,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT21F001 DD DSN=&FT21,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=*.FT01F001
//GC.FT23F001 DD DSN=*.STEP4.GC.FT22F001,DISP=(OLD,KEEP)
//GC.FT24F001 DD DSN=*.STEP1.GC.FT04F001,DISP=(OLD,KEEP)
// ( REPLACE THIS CARD WITH THE INPUT DATA TO THE FINAL P.FLOW PROG. )
//
//

```

4.2 JCL Setup for Executing the Programs Already Stored on an External Unit.

All program steps are stored in the volume "CSLB30."

(a) The Potential-Flow Program Step has the data set name

"DAC.EOH3.DPM.J1HB.V3."

Card
Column

```

0      1      2      3      4      5      6      7
123456789012345678901234567890123456789012345678901234567890123
//STEP1 EXEC  FORTGO,REGION=380K
//STEPL1B DD  DSN=DAC.EOH3.DPM.J1HB.V3,DISP=(SHR,PASS),UNIT=3330-1,
//           VOL=SER=CSLB30
//GO.FT01F001 DD DSNNAME=&FT01,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT02F001 DD DSN=RUNCASE.UVDATA,UNIT=TAPE16,DISP=(NEW,PASS),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1),
//           LABEL=(1,SL,RETPD=180)
//GO.FT03F001 DD DSNNAME=&FT03,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT04F001 DD DSN=RUNCASE.GEOMDATA,UNIT=TAPE16,DISP=(NEW,PASS),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1),
//           LABEL=(1,SL,RETPD=180)
//GO.FT07F001 DD SYSOUT=B
//GO.FT08F001 DD DSNNAME=&FT08,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT09F001 DD DSNNAME=&FT09,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT10F001 DD DSNNAME=&FT10,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT11F001 DD DSNNAME=&FT11,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT12F001 DD DSNNAME=&FT12,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT13F001 DD DSNNAME=&FT13,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT14F001 DD DSNNAME=&FT14,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT15F001 DD DSNNAME=&FT15,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT16F001 DD DSNNAME=&FT16,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT17F001 DD DSNNAME=&FT17,UNIT=SYSDA,SPACE=(TRK,(10,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT18F001 DD DSNNAME=&FT18,UNIT=SYSDA,SPACE=(TRK,(10,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT19F001 DD DSNNAME=&FT19,UNIT=SYSDA,SPACE=(TRK,(10,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT21F001 DD DSN=RUNCASE.FLOWDATA,UNIT=TAPE16,DISP=(NEW,PASS),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1),
//           LABEL=(1,SL,RETPD=180)
//GO.FT23F001 DD DSN=&FT23,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT24F001 DD DSN=&FT24,UNIT=SYSDA,SPACE=(TRK,(50,5)),
//           DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.SYSIN DD *
/* ( REPLACE THIS CARD WITH THE INPUT DATA TO POTENTIAL FLOW PROG. )

```


- (b) The streamline Calculation Program has the data set name
"DAC.EOH3.DPM.J1HB.STREAM."

Card
Column

0 1 2 3 4 5 6 7
123456789012345678901234567890123456789012345678901234567890123

```
//STEP2 EXEC FORTGO,REGION=250K
//STEPLIB DD DSN=DAC.EOH3.DPM.J1HB.STREAM,DISP=(SHR,PASS),
// UNIT=3330-1,VOL=SER=CSLB30
//GO.FT01F001 DD DSN=OUTDATA.TL4EY,UNIT=TAPE16,DISP=(NEW,PASS),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=4000),
// LABEL=(1,SL,RETPD=180)
//GO.FT02F001 DD DSN=&FT02,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT03F001 DD DSN=&FT03,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT04F001 DD DSN=&FT04,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT07F001 DD SYSOUT=R
//GO.FT10F001 DD DSN=DAC.EOH3.DPM.J1HB.RUNCASE,UNIT=3330-1,
// DCB=(DSORG=DA,BUFNO=1),VOL=SER=CSLB30,DISP=(NEW,PASS)
// SPACE=(100,(2000))
//GO.FT15F001 DD DSN=*.STEP1.GO.FT02F001,DISP=(OLD,PASS)
//GO.FT16F001 DD DSN=*.STEP1.GO.FT04F001,DISP=(OLD,PASS)
//GO.FT21F001 DD DSN=*.STEP1.GO.FT21F001,DISP=(OLD,KEEP)
//GO.SYSIN DD *
```

(REPLACE THIS CARD WITH THE INPUT DATA TO THE STREAMLINE PROG.)

/*

- (c) The Boundary-Layer Program has the data set name "DAC.EOH3.DPM.J1HB.L4EY."

0 1 2 3 4 5 6 7
123456789012345678901234567890123456789012345678901234567890123

```
//STEP3 EXEC FORTGO,REGION=200K
//STEPLIB DD DSN=DAC.EOH3.DPM.J1HB.L4EY,DISP=(SHR,PASS),
// UNIT=3330-1,VOL=SER=CSLB30
//GO.FT01F001 DD DSN=*.STEP2.GO.FT01F001,DISP=(OLD,KEEP)
//GO.FT02F001 DD DSN=DSTAR.FL4EY,UNIT=TAPE16,DISP=(NEW,PASS),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=4000),
// LABEL=(1,SL,RETPD=180)
//GO.FT03F001 DD DSN=*.STEP1.GO.FT02F001,DISP=(OLD,PASS)
//GO.FT04F001 DD DSN=*.STEP1.GO.FT04F001,DISP=(OLD,PASS)
//GO.FT10F001 DD DSN=*.STEP2.GO.FT10F001,DISP=(OLD,PASS)
//GO.FT07F001 DD SYSOUT=R
//GO.SYSIN DD *
```

(REPLACE THIS CARD WITH THE INPUT DATA TO THE BOUNDARY LAYER PROG)

/*

- (d) The Back Interpolation Program has the data set name "DAC.EOH3.DPM.J1HB.BACKINP."

```
//STEP4 EXEC FORTGO,REGION=220K
//STEPLIB DD DSN=DAC.EOH3.DPM.J1HB.BACKINT,DISP=(SHR,PASS),
// UNIT=3330-1,VOL=SER=CSLB30
//GO.FT01F001 DD DSN=*.STEP3.GO.FT02F001,DISP=(OLD,KEEP)
//GO.FT02F001 DD DSN=&FT02,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT03F001 DD DSN=&FT03,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT04F001 DD DSN=&FT04,UNIT=SYSDA,SPACE=(TRK,(50,10)),
// DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1)
//GO.FT07F001 DD SYSOUT=R
//GO.FT10F001 DD DSN=DAC.EOH3.DPM.J1HB.RUNCASE,UNIT=3330-1,
// DCB=(DSORG=DA,BUFNO=1),VOL=SER=CSLB30,DISP=(OLD,KEEP),
// SPACE=(100,(2000))
//GO.FT16F001 DD DSN=*.STEP1.GO.FT04F001,DISP=(OLD,PASS)
//GO.FT20F001 DD DSN=*.STEP1.GO.FT02F001,DISP=(OLD,KEEP)
//GO.FT22F001 DD DSN=DSTAR.TJ1HB,UNIT=TAPE16,DISP=(NEW,PASS),
// DCB=(RECFM=VBS,BLKSIZE=6447,BUFNO=1),
// LABEL=(1,SL,RETPD=180)
//GO.SYSIN DD *
```

(REPLACE THIS CARD WITH THE INPUT DATA TO THE BACK INTERP. PROG.)

/*

5.0 SAMPLE TEST CASE

The sample test case is an eight-strip swept wing with 30 on-body elements and one wake element per strip. The test case is run at an angle of attack of 8.22° with one plane of symmetry.

The input data and partial output are included. Due to the size of the output from the programs, only the output for the first strip is presented here.

5.1 Input Data

(a) Input Data to the Potential Flow Program. Initial Calculation.

0								1								2								3								4								5								6								7							
1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8								
NACA SWEPT WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL.SYM. P.KUTTA																																																															
NACA 1 1 1 1.0 1.0 1.0																																																															
0.989707 0. 0.143106																																																															
30 1 8 0																																																															
0. 2.17 2.80 4.70 6.10 10.00																																																															
8.40 6.80 5.70 0.00																																																															
73.545 46.67 .0 21 72.7162 46.67 -.0752136																																																															
71.8708 46.67 -.149184 70.1221 46.67 -.3016832																																																															
68.2966 46.67 -.4585336 66.3883 46.67 -.602952																																																															
64.3909 46.67 -.7187768 62.2982 46.67 -.7848736																																																															
60.1039 46.67 -.7784504 57.7978 46.67 -.7046872																																																															
55.3756 46.67 -.5412064 54.1159 46.67 -.39886																																																															
53.4756 46.67 -.2913232 53.1503 46.67 -.2119656																																																															
52.9555 46.67 -.1394456 52.825 46.67 .0																																																															
52.9555 46.67 .1394456 53.1503 46.67 .2119656																																																															
53.4756 46.67 .2913232 54.1159 46.67 .39886																																																															
55.3756 46.67 .5412064 57.7978 46.67 .7046872																																																															
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68.2966 46.67 .4585336 70.1221 46.67 .3016832																																																															
71.8708 46.67 .149184 72.7162 46.67 .0752136																																																															
73.545 46.67 .0 74.3738 46.67 .0																																																															
72.05 44.5 .0 1 71.1828 44.5 -.078698																																																															
70.2983 44.5 -.156096 68.4685 44.5 -.315661																																																															
66.5585 44.5 -.479778 64.5617 44.5 -.630888																																																															
62.4718 44.5 -.752079 60.2821 44.5 -.821238																																																															
57.9862 44.5 -.814518 55.5732 44.5 -.737337																																																															
53.0388 44.5 -.566282 51.7207 44.5 -.41734																																																															
51.0508 44.5 -.304821 50.7147 44.5 -.221786																																																															
50.5066 44.5 -.145906 50.37 44.5 .0																																																															
50.5066 44.5 .145906 50.7147 44.5 .221786																																																															
51.0508 44.5 .304821 51.7207 44.5 .41734																																																															
53.0388 44.5 .566282 55.5732 44.5 .737337																																																															
57.9862 44.5 .814518 60.2821 44.5 .821238																																																															
62.4718 44.5 .752079 64.5617 44.5 .630888																																																															
66.5585 44.5 .479778 68.4685 44.5 .315661																																																															
70.2983 44.5 .156097 71.1828 44.5 .078689																																																															
72.05 44.5 .0 72.9172 44.5 .0																																																															
70.13 41.7 .0 1 69.2128 41.7 -.083236																																																															
68.2773 41.7 -.165096 66.3420 41.7 -.333861																																																															
64.3218 41.7 -.507441 62.21 41.7 -.667263																																																															
59.9995 41.7 -.795442 57.6836 41.7 -.868588																																																															
55.2553 41.7 -.86148 52.7032 41.7 -.779849																																																															
50.0227 41.7 -.598932 48.6285 41.7 -.441403																																																															
47.92 41.7 -.322396 47.56 41.7 -.234574																																																															
47.3445 41.7 -.154319 47.2 41.7 .0																																																															
47.3445 41.7 .154319 47.56 41.7 .234574																																																															
47.92 41.7 .322396 48.6285 41.7 .441403																																																															
50.0227 41.7 .598932 52.7032 41.7 .779849																																																															
55.2553 41.7 .861480 57.6836 41.7 .868588																																																															
59.9995 41.7 .795442 62.21 41.7 .667263																																																															
64.3218 41.7 .507441 66.3420 41.7 .333861																																																															
68.2773 41.7 .165096 69.2128 41.7 .083236																																																															
70.13 41.7 .0 71.0472 41.7 .0																																																															
66.9 37.0 .0 1 65.8992 37.0 -.090823																																																															
64.8784 37.0 -.180144 62.7667 37.0 -.364291																																																															
60.5624 37.0 -.553693 58.2581 37.0 -.728082																																																															
55.8462 37.0 -.867944 53.3191 37.0 -.947758																																																															
50.6695 37.0 -.940001 47.8848 37.0 -.85093																																																															
44.96 37.0 -.653522 43.4387 37.0 -.481635																																																															
42.6656 37.0 -.351781 42.2728 37.0 -.255955																																																															
42.0376 37.0 -.168385 41.98 37.0 .0																																																															
42.0376 37.0 .168385 42.2728 37.0 .255955																																																															

(continued)

0	1	2	3	4	5	6	7
1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890
42.6656	37.0	.351781	43.4387	37.0	.481635		
44.96	37.0	.653522	47.8848	37.0	.85093		
50.6695	37.0	.940001	53.3191	37.0	.947758		
55.8462	37.0	.867944	58.2581	37.0	.728082		
60.5624	37.0	.553693	62.7667	37.0	.364291		
64.8784	37.0	.180144	65.8992	37.0	.090823		
66.9	37.0	.0	67.9008	37.0	.0		
62.71	30.90	.0	61.6008	30.90	-.1006599		
60.4694	30.90	-.199656	58.1290	30.90	-.4037488		
55.6860	30.90	-.6136649	53.1321	30.90	-.806943		
50.4589	30.90	-.9619537	47.6582	30.90	-1.050412		
44.7215	30.90	-1.0418161	41.6352	30.90	-.9430973		
38.3936	30.90	-.7243076	36.7076	30.90	-.5338025		
35.8507	30.90	-.3898838	35.4154	30.90	-.2836779		
35.1547	30.90	-.1866229	34.98	30.90	.0		
35.1547	30.90	.1866229	35.4154	30.90	.2836779		
35.8507	30.90	.3898838	36.7076	30.90	.5338025		
38.3936	30.9	.7243076	41.6352	30.9	.9430973		
44.7215	30.9	1.0418161	47.6582	30.9	1.0504124		
50.4589	30.9	.9616537	53.1321	30.9	.806943		
55.6860	30.9	.6136649	58.1290	30.9	.4037488		
60.4694	30.9	.199656	61.6008	30.9	.1006599		
62.71	30.9	.0	63.8192	30.9	.0		
55.83	20.9	.0	54.5432	20.9	-.1167771		
53.2307	20.9	-.231624	50.5155	20.9	-.4683952		
47.6813	20.9	-.7119221	44.7185	20.9	-.936147		
41.6173	20.9	-1.115977	38.3681	20.9	-1.2186		
34.9613	20.9	-1.2086269	31.3808	20.9	-1.094102		
27.6201	20.9	-.8402804	25.6642	20.9	-.6192725		
24.6701	20.9	-.4523102	24.1651	20.9	-.3290991		
23.8627	20.9	-.2165041	23.66	20.9	.0		
23.8627	20.9	.2165041	24.1651	20.9	.3290991		
24.6701	20.9	.4523102	25.6642	20.9	.6192725		
27.6201	20.9	.8402804	31.3808	20.9	1.0941017		
34.9613	20.9	1.2086269	38.3681	20.9	1.2185996		
41.6173	20.9	1.1159773	44.7185	20.9	.936147		
47.6813	20.9	.7119221	50.5155	20.9	.4683952		
53.2307	20.9	.231624	54.5432	20.9	.1167771		
55.83	20.9	.0	57.1168	20.9	.0		
50.06	12.5	.0	48.6236	12.5	-.1303533		
47.1585	12.5	-.258552	44.1277	12.5	-.5228496		
40.9640	12.5	-.7946883	37.6567	12.5	-1.044981		
34.1950	12.5	-1.245718	30.5681	12.5	-1.360271		
26.7652	12.5	-1.349139	22.7684	12.5	-1.221299		
18.5705	12.5	-.9379692	16.3872	12.5	-.6912675		
15.2776	12.5	-.5048946	14.7138	12.5	-.3673593		
14.3762	12.5	-.2416743	14.15	12.5	.0		
14.3762	12.5	.2416743	14.7138	12.5	.3673593		
15.2776	12.5	.5048946	16.3872	12.5	.6912675		
18.5705	12.5	.9379692	22.7684	12.5	1.221299		
26.7652	12.5	1.349139	30.5681	12.5	1.36027		
34.1950	12.5	1.245718	37.6567	12.5	1.044981		
40.9640	12.5	.7946883	44.1277	12.5	.5228496		
47.1585	12.5	.258552	48.6236	12.5	.1303533		
50.06	12.5	.0	51.4964	12.5	.0		
45.39	5.7	.0	43.8324	5.7	-.1413522		
42.2436	5.7	-.280368	38.9571	5.7	-.5669664		
35.5265	5.7	-.8617422	31.9401	5.7	-1.133154		
28.1863	5.7	-1.350829	24.2534	5.7	-1.475047		
20.1296	5.7	-1.462976	15.7956	5.7	-1.324349		
11.2435	5.7	-1.017113	8.8760	5.7	-.749595		
7.6727	5.7	-.5474964	7.0614	5.7	-.3983562		
6.6953	5.7	-.2620662	6.45	5.7	.0		
6.6953	5.7	.2620662	7.0614	5.7	.3983562		
7.6727	5.7	.5474964	8.8760	5.7	.749595		
11.2435	5.7	1.0171128	15.7956	5.7	1.3243494		
20.1296	5.7	1.4629759	24.2534	5.7	1.4750472		
28.1863	5.7	1.3508286	31.9401	5.7	1.133154		
35.5265	5.7	.8617422	38.9571	5.7	.5669664		
42.2436	5.7	.280368	43.8324	5.7	.1413522		
45.39	5.7	.0	46.9476	5.7	.0		

(continued)

0								1								2								3								4								5								6								7																						
1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8																							
41.47								0.0							.0								1								39.8112								0.0								-.1505361																															
38.1192								0.0							-.298584																34.6192								0.0								-.6038																															
30.9656								0.0							-0.9177311																27.1463								0.0								-1.20678																															
23.1486								0.0							-1.438594																18.9601								0.0								-1.570884																															
14.5684								0.0							-1.558028																9.9528								0.0								-1.410395																															
5.1050								0.0							-1.083196																2.5836								0.0								-.798298																															
1.3022								0.0							-.5830682																.6511								0.0								-.4242381																															
.2613								0.0							-.2790931																.0								0.0								.0																															
.2613								0.0							.2790931																.6511								0.0								.4242381																															
1.3022								0.0							.5830682																2.5835								0.0								.798298																															
5.1050								0.0							1.0831964																9.9528								0.0								1.4103947																															
14.5684								0.0							1.558028																18.9601								0.0								1.570884																															
23.1486								0.0							1.4385943																27.1463								0.0								1.206777																															
30.9656								0.0							.9177311																34.6192								0.0								.6038																															
38.1192								0.0							.298584																39.8112								0.0								.1505361																															
41.47								0.0							.0																43.1288								0.0								.0																															

(b) Input Data to the Streamline Calculation Program.

```

EIGHT STRIPS NACA SWEEP WING. ALPHA=8.2. STREAMLINE CALCULATION.
0      EIGHT STRIPS NACA SWEEP WING.
10 1 0.0      SET NO. 1 MACH = 0.0
00 1 8.23 0.0 ALPHA-BETA SET NO.1
10 1200      THIS IS THE LOWER SURFACE REGION.
12 2 8.23 0.0 ALPHA-BETA SET NO.2
10 1200      THIS IS THE UPPER SURFACE REGION.
1      EIGHT STRIPS NACA SWEEP WING.
11 1 0.0      SET NO.1 MACH = 0.0
01 1 8.23 0.0 ALPHA-BETA SET NO.1
11 12 1      THIS IS THE LOWER SURFACE REGION.
11 2 8.23 0.0 ALPHA-BETA SET NO.2
11 12 1      THIS IS THE UPPER SURFACE REGION.
0 1 1 1000 1      0      0.999      0.010      0.0010
1 8      STREAMLINES FOR THE LOWER SURFACE.
1 1100      0.02
1 1100      0.02
1 1100      0.02
1 1100      0.02
1 1100      0.02
1 1100      0.02
1 1100      0.02
1 1100      0.02
1 1 2 1000 1      0      0.999      0.010      0.0010
1 8      STREAMLINES FOR THE UPPER SURFACE.
1 1100      0.02
1 1100      0.02
1 1100      0.02
1 1100      0.02
1 1100      0.02
1 1100      0.02
1 1100      0.02
1 1100      0.02
EIGHT STRIPS NACA SWEEP WING.
223.3      6700000.0      12.0

```

(c) Input Data to the Boundary-Layer Calculation Program.

Card
Column

0 1 2 3 4 5 6 7
12345678901234567890123456789012345678901234567890123

```

16      1      2      0      0      1
 9
 9
 9
 9
 9
 9
10
10
10
10
10
10
 9
 9
 9
 9

```

(d) Input Data to the Back Interpolation Program.

```

NACA 8 STRIP SWEEP WING. BACK INTERPOLATION. BOTH SURFACES.      2
 1      2      3      4      20      22      30      1      0
 1      8      504      1      15      0.0      0.0      42.1256      21.0475
 0.0      8      1167      16      30      41.713      83.4866      -47.0485      -23.5071
 2      0.0      8      1167      16      30      41.713      83.4866      -47.0485      -23.5071
65      0      517
62      0      582
63      0      644
71      0      707
69      0      778
66      0      847
59      0      913
18      1      972
18      1      1180
43      0      1198
40      0      1241
40      0      1281
41      0      1321
42      0      1362
42      0      1404
41      0      1446

```

(e) Input Data to the Final Calculation in the Potential Flow Program.

```

NACA SWEEP WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL.SYM. P.KUTTA
NACA 1      1      1      1      1      1.0      0.0      1.0
0.989707 0.      0.143106
30      1      8      0
 0.      2.17      2.80      4.70      6.10      10.00
 8.40      6.80      5.70      0.00

```

5.2 Output Data

The output data from the test case consists of the output from these programs:

1. The initial potential-flow calculation (pp 41 - 49).
2. The streamline calculation (pp 50 - 68).
3. The small cross-flow boundary-layer calculation (pp 69 - 73).
4. The final potential-flow computation (pp 74 - 82).

Output of the first strip from this eight-strip test case is used here as a sample. Similarly, the first streamline output of the lower surface of the wing is selected in both streamline calculation and the boundary-layer calculation.

PROGRAM J1HA
CASE NO. NACA

DOUGLAS AIRCRAFT COMPANY
LONG BEACH DIVISION
TUESDAY, NOV 30, 1976

PAGE 1.

NACA SWEPT WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL.SYM. P.KUTTA

```

CASE ID  SECTIONS  NACA
LIFTING  1
KUTTA    1
OFF - BODY POINTS  0
UNIFORM  0
IGNORE ELEMENT  0
MOMENT INPUT  0
SPECIAL LAST WAKE CALCULATION  0
PIECEWISE EXECUTION  0
PIECEWISE LINEAR VORTICITY  0
STEP FUNCTION VORTICITY  1
SYMMETRY  1
ROUNDARY LAYER CALCULATION  -1
INTERMEDIATE OUTPUT  0
PARABOLIC VORTICITY OPTION  0
( NONZEROS IMPLIED OPTIONS WERE SELECTED )

```

FOOT CONVERTER FACTOR INPUT ---- 1.0

COMPONENTS OF THE UNIFORM ONSET FLOWS
(1) 0.989707, 0.0 , 0.143106

OTHER INPUT INFORMATION WILL BE WRITTEN ELSEWHERE IN THE OUTPUT.

PAGE 2.

PROGRAM JIHA
CASE NO. NACA

DCUGLAS AIRCRAFT DIVISION COMPANY
LCMC BEACH NOV 30, 1976
TUESDAY, A=8.22, 30 SCURCE, 1 WAKE, 1 PL.SYM. P.KUTTA

----- * -----

BEGIN THE SUBROUTINE INPUT . TIME IS 0.029 SEC.
BEGIN THE FORMATION OF ELEMENTS. TIME IS 0.071 SEC.

PROGRAM JIHA
CASE NO. NACA

DCUGLAS AIRCRAFT COMPANY
LONG BEACH, NOV 30, 1976

NACA SWEEP WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL.SYM. P.KUTTA

N	M	X	Y	Z	X	Y	Z	X	Y	Z	NX	NY	NZ	XO	YO	ZO	D	T	A	TYPE OF ELEMENT
1	1	73.544958	46.665558	0.0	72.716202	46.665558	0.0	71.182800	44.500000	0.0	0.090204	-0.062146	-0.093982	72.367767	45.576797	-0.133484	2.2352E-07	3.2086E+00	1.8513E+00	LIFT
2	2	72.716202	46.665558	-0.075214	71.182800	44.500000	-0.075214	70.298294	44.500000	-0.156096	0.087012	-0.059888	-0.094405	71.511154	45.576797	-0.114817	1.9334E-06	1.8875E+00	1.8875E+00	
3	3	71.182800	46.665558	-0.149184	70.298294	44.500000	-0.149184	68.468506	44.500000	-0.315861	0.086721	-0.059888	-0.094405	70.182800	45.576797	-0.230695	2.3648E-07	3.5043E+00	3.5043E+00	
4	4	70.298294	46.665558	-0.315861	68.468506	44.500000	-0.315861	66.558502	44.500000	-0.475778	0.085461	-0.059888	-0.094405	68.355011	45.576797	-0.388930	1.6093E-06	4.0150E+00	4.0150E+00	
5	5	69.256600	45.665558	-0.458534	66.558502	44.500000	-0.458534	64.561707	44.500000	-0.630888	0.075365	-0.050617	-0.095871	66.444534	45.576797	-0.543130	1.6093E-06	4.2200E+00	4.2200E+00	
6	6	68.388306	44.665558	-0.602952	64.561707	44.500000	-0.602952	62.471802	44.500000	-0.752079	0.057854	-0.035854	-0.097681	64.446091	45.576797	-0.676289	1.0133E-06	4.4450E+00	4.4450E+00	
7	7	67.350900	43.665558	-0.718177	62.471802	44.500000	-0.718177	60.232104	44.500000	-0.821238	0.031566	-0.012578	-0.099423	62.353302	45.576797	-0.763373	4.3958E-07	4.6471E+00	4.6471E+00	
8	8	66.298203	42.665558	-0.784414	60.232104	44.500000	-0.784414	57.986206	44.500000	-0.821238	-0.002927	0.016474	-0.099806	60.158805	45.576797	-0.799906	3.1292E-07	4.8273E+00	4.8273E+00	
9	9	65.103857	41.665558	-0.844414	57.986206	44.500000	-0.844414	55.573196	44.500000	-0.821238	-0.019333	0.047757	-0.099806	57.857056	45.576797	-0.799906	1.0543E-06	5.0237E+00	5.0237E+00	
10	10	57.797806	46.665558	-0.704687	55.573196	44.500000	-0.704687	53.038803	44.500000	-0.566282	0.031933	-0.047757	-0.099806	55.437744	45.576797	-0.537487	4.5757E-07	5.1287E+00	5.1287E+00	
11	11	55.375555	44.665558	-0.541206	53.038803	44.500000	-0.541206	51.720703	44.500000	-0.417340	-0.067103	0.083750	-0.094225	53.553802	45.576797	-0.431034	2.9802E-07	5.2322E+00	5.2322E+00	
12	12	54.115206	43.665558	-0.417340	51.720703	44.500000	-0.417340	49.500000	44.500000	-0.266282	-0.111113	0.131253	-0.085080	51.553802	45.576797	-0.353146	1.4193E-06	5.3538E+00	5.3538E+00	
		53.475601	42.665558	-0.291323	49.500000	44.500000	-0.291323	47.200000	44.500000	-0.131253	-0.018781	0.162687	-0.098637	52.581645	45.576797	-0.353146	2.3022E-06	5.4676E+00	5.4676E+00	

PROGRAM JIHA DOUGLAS AIRCRAFT COMPANY
CASE NO. NACA LCNG BEACH DIVISION
TUESDAY, NCV 30, 1976
NACA SWEEP WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL.SYM. P.KUTTA

N	M	X	Y	Z	X	Y	Z	X	Y	Z	NX	NY	NZ	X ₀	Y ₀	Z ₀	P	A	TYPE OF ELEMENT
1	13	53.475601	53.156259	50.714706	51.050797	-0.230079	52.091080	2.4332E-04						52.091080	45.573964	-0.257506	3.5123E+00		LIFT
		46.665558	-0.211866	-0.221786	-0.304821	-0.937045	-0.257506	7.6581E-01						-0.257506	51.818832	45.573964	3.3668E-04		
	14	53.156259	52.955505	50.506607	50.714706	-0.311739	51.818832	3.3668E-04						51.818832	45.573964	-0.257506	3.3668E-04		
		46.665558	-0.211866	-0.221786	-0.304821	-0.937045	-0.257506	7.6581E-01						-0.257506	51.818832	45.573964	3.3668E-04		
	15	52.955505	52.824557	50.369995	50.506607	-0.311739	51.818832	3.3668E-04						51.818832	45.573964	-0.257506	3.3668E-04		
		46.665558	0.0	0.0	0.0	0.0	0.0	0.0						51.818832	45.573964	-0.257506	3.3668E-04		
	16	52.824557	52.955505	50.506607	50.714706	-0.311739	51.818832	3.3668E-04						51.818832	45.573964	-0.257506	3.3668E-04		
		46.665558	0.0	0.0	0.0	0.0	0.0	0.0						51.818832	45.573964	-0.257506	3.3668E-04		
	17	52.955505	52.824557	50.369995	50.506607	-0.311739	51.818832	3.3668E-04						51.818832	45.573964	-0.257506	3.3668E-04		
		46.665558	0.0	0.0	0.0	0.0	0.0	0.0						51.818832	45.573964	-0.257506	3.3668E-04		
	18	53.156259	53.475601	51.050797	51.818832	-0.230079	52.091080	2.4332E-04						52.091080	45.573964	-0.257506	3.5123E+00		
		46.665558	0.291323	0.304821	0.3221786	0.937045	-0.257506	7.6581E-01						-0.257506	51.818832	45.573964	3.3668E-04		
	19	53.475601	54.115206	51.720703	51.050797	-0.152687	52.581665	2.7232E-06						52.581665	45.573964	-0.257506	3.3668E-04		
		46.665558	0.398260	0.411340	0.430821	0.988637	-0.257506	7.6581E-01						-0.257506	51.818832	45.573964	3.3668E-04		
	20	53.115906	55.375525	53.038803	51.720703	-0.111313	53.553302	1.0729E-06						53.553302	45.573964	-0.257506	3.3668E-04		
		46.665558	0.541206	0.566282	0.411340	0.988637	-0.257506	7.6581E-01						-0.257506	51.818832	45.573964	3.3668E-04		
	21	55.375525	57.797806	55.573196	53.038803	-0.067103	55.437744	1.4901E-08						55.437744	45.573964	-0.257506	3.3668E-04		
		46.665558	0.704667	0.737337	0.566282	0.994225	-0.257506	7.6581E-01						-0.257506	51.818832	45.573964	3.3668E-04		
	22	57.797806	60.103857	57.586206	55.573196	-0.031933	57.357056	1.5274E-07						57.357056	45.573964	-0.257506	3.3668E-04		
		46.665558	0.778450	0.814518	0.737337	0.998349	-0.257506	7.6581E-01						-0.257506	51.818832	45.573964	3.3668E-04		
	23	60.103857	62.298203	60.282104	57.586206	-0.002927	60.159925	2.5802E-08						60.159925	45.573964	-0.257506	3.3668E-04		
		46.665558	0.78474	0.821238	0.814518	0.995806	-0.257506	7.6581E-01						-0.257506	51.818832	45.573964	3.3668E-04		
	24	62.298203	64.390900	62.471302	60.282104	0.031566	62.353302	1.2219E-06						62.353302	45.573964	-0.257506	3.3668E-04		
		46.665558	0.718714	0.7520	0.821238	-0.012578	62.353302	1.2219E-06						-0.257506	51.818832	45.573964	3.3668E-04		

PROGRAM J11A AIRCRAFT COMPANY
CASE NO. NACA BEACH DIVISION
TUESDAY, NCV 30, 1976

NACA SWEPT WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL.SYM. P.KUTTA

N	M	X	Y	Z	X	Y	Z	X	Y	Z	NX	NY	NZ	XO	YO	ZO	D	T	A	TYPE OF ELEMENT
1	25	64.390500	46.265558	0.718777	66.388306	64.561707	44.500000	62.471802	44.500000	0.752079	0.057854	-0.035854	0.997681	64.446091	45.576797	0.675239	5.58795E-07	4.48000E+00	4.44500E+00	LIFT
26	66.388306	46.265558	0.602952	68.256600	66.558502	44.500000	64.561707	64.561707	44.500000	0.630888	0.075365	-0.050617	0.995871	66.444534	45.576797	0.543130	1.00965E-06	4.32300E+00	4.25466E+00	
27	63.256600	46.265558	0.602952	70.122101	68.468506	44.500000	64.561707	66.558502	44.500000	0.479778	0.085461	-0.058716	0.994610	68.355011	45.576797	0.388990	1.78815E-06	4.17615E+00	4.07950E+00	
28	70.122101	46.265558	0.301683	71.870806	70.298296	44.500000	64.561707	68.468506	44.500000	0.315661	0.086721	-0.056766	0.994444	70.132397	45.576797	0.230696	2.53305E-06	3.90435E+00	3.83705E-06	
29	71.870806	46.265558	0.145184	72.716202	71.182800	44.500000	64.561707	70.298296	44.500000	0.156097	0.087018	-0.059894	0.994405	71.511154	45.576797	0.114815	3.24995E+00	1.88755E+00	3.83705E-06	
30	72.716202	46.265558	0.075214	73.544558	72.500000	44.500000	64.561707	71.182800	44.500000	0.078689	0.090198	-0.062144	0.993983	72.367767	45.576797	0.033482	2.35815E-06	3.20865E+00	1.85135E+00	
31	73.544558	46.265558	0.000000	74.373795	72.517206	44.500000	64.561707	72.500000	44.500000	0.000000	0.000000	0.000000	1.000000	73.215927	45.576797	0.000000	0.000000	3.17955E+00	1.84025E+00	WAKE
2	1	72.050000	46.500000	0.000000	71.182800	69.212799	41.565997	70.130005	41.565997	0.000000	0.090206	-0.061855	0.994001	70.634796	43.086314	-0.004344	1.23685E-06	3.58705E+00	2.51332E+00	LIFT
2	2	71.182800	44.500000	0.078689	70.298296	68.272298	41.565997	69.212799	41.565997	-0.083236	0.087016	-0.059610	0.994422	69.733444	43.086314	0.0120813	8.60545E-07	4.03805E+00	2.56235E+00	
3	3	70.298296	44.500000	0.156097	68.468506	66.341995	41.565997	68.272298	41.565997	-0.165096	0.086721	-0.059397	0.994460	68.335807	43.086314	0.0242742	7.15265E-07	4.45015E+00	5.30055E+00	
4	4	63.468506	44.500000	0.315661	66.558502	64.321793	41.565997	66.341995	41.565997	-0.333861	0.085462	-0.058442	0.994626	66.412491	43.086314	-0.0409292	1.31135E-06	5.00725E+00	5.53205E+00	
5	5	46.558502	44.500000	0.479778	64.561707	62.210007	41.565997	64.321793	41.565997	-0.507441	0.075367	-0.050364	0.995883	64.402267	43.086314	-0.0571491	3.15990E-06	4.17545E+00	7.77585E+00	

PROGRAM JIHA
CASE NO. NACA

DOUGLAS AIRCRAFT COMPANY
LONG BEACH DIVISION
TUESDAY, NOV 30, 1976

PAGE 27.

NACA SWEPT WING, 8 STRIPS, A=8.22, 30 SCURCE, 1 WAKE, 1 PL.SYM. P.KUTTA
UNIFORM ONSET FLOW = (0.589707E+00, 0.0 , 0.143106E+00)

FINAL OUTPUT FOR THE FOLLOWING ANGLE OF ATTACK

(0.589707, 0.0 0.143106)

BEST AVAILABLE COPY

PAGE 28.

PROGRAM JIHA
CASE NO. NACA

DOUGLAS AIRCRAFT COMPANY
LONG BEACH, CALIF. 90801
TUESDAY, NOV 30, 1976

NACA SHEPT WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 MAKE, 1 PL.SYM. P.KUTTA
UNIFORM CNSET FLOW = (0.589707E+00, 0.0 , 0.143106E+00)

N	M	ON - BCDY			PCINTS			FINAL			OUTPUT			NX			SIG		
		VX	VO	ZO	VT	VSQ	CP	DCX	DCY	DCZ	NX	NY	NZ	NX	NY	NZ	AREA	AREA	AREA
1	1	72.367767 45.576757 -0.038464	0.920055 0.081061 0.078433	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776	0.926943 0.859224 0.140776
2	2	71.511154 45.576757 -0.114817	0.961679 0.128246 0.078430	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884	0.973199 0.947116 0.052884
3	3	70.163807 45.576757 -0.230695	0.934394 0.218220 0.073066	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705	1.009805 1.019705 -0.019705
4	4	68.355011 45.576757 -0.388888	1.004082 0.281521 0.069665	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285	1.045124 1.092285 -0.092285
5	5	65.444534 45.576757 -0.543120	1.012349 0.313622 0.060679	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889	1.061550 1.126889 -0.126889
6	6	64.446091 45.576757 -0.676289	1.015050 0.330298 0.046598	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631	1.068471 1.141631 -0.141631
7	7	62.352302 45.576757 -0.769373	1.011863 0.347382 0.027595	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301	1.070188 1.145301 -0.145301
8	8	60.155805 45.576757 -0.755006	0.996553 0.373315 0.044361	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500	1.066180 1.132500 -0.132500
9	9	57.857056 45.576757 -0.755006	0.973117 0.402201 0.011879	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863	1.053025 1.108863 -0.108863
10	10	55.437744 45.576757 -0.537487	0.925033 0.439529 0.025432	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629	1.025002 1.050629 -0.050629
11	11	53.553802 45.576757 -0.461004	0.872209 0.448480 0.038784	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614	0.941522 0.963386 0.036614

PROGRAM JIHA
CASE NO. NACA

DOUGLAS AIRCRAFT COMPANY
LCNCG BEACH, NCV 30, 1976

NACA SWEEP WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL-SYM. P.KUTTA
UNIFORM ONSET FLOW = (0.595707E+00, 0.0 , 0.143106E+00)

ON - BCDY POINTS FINAL OUTPUT

N	M	XO YO ZO	VX VY VZ	VT VTSQ CP	DCX DCY DCZ	NX NY NZ	SIG VN AREA
1	12	52.531665 45.576813 -0.353146	0.747094 0.477825 -0.032808	0.887436 0.787542 0.212458	0.841857 0.538433 -0.036970	-0.162687 0.187817 -0.958637	0.154319 -0.000019 1.467604
13		52.091080 45.578564 -0.257506	0.581113 0.604600 0.026836	0.830020 0.703954 0.296046	0.692609 0.720603 0.031985	-0.230079 0.262701 -0.937045	0.160093 -0.000019 0.765805
14		51.918822 45.573502 -0.175819	0.392131 0.791562 0.186705	0.902920 0.815228 0.184772	0.434302 0.876711 0.206784	-0.321739 0.365361 -0.873488	0.155595 -0.000019 0.500452
15		51.654938 45.576732 -0.071350	0.178215 1.014112 1.035309	1.460153 2.132046 -1.132046	0.122052 0.694334 0.709041	-0.552892 0.636812 -0.526899	0.147071 -0.000020 0.550022
16		51.654938 45.576732 0.071350	1.281613 -0.242063 1.661635	2.112392 4.462158 -3.462158	0.606715 -0.114592 0.786617	-0.552892 0.636812 0.526899	-0.041480 -0.000045 0.550021
17		51.918822 45.573502 0.175819	1.522354 -0.545828 0.800115	1.829731 3.347914 -2.347914	0.848405 -0.298311 0.437286	-0.321739 0.365361 0.873488	-0.116154 -0.000033 0.500452
18		52.091080 45.578564 0.257506	1.453803 -0.425370 0.476219	1.587850 2.521265 -1.521265	0.915580 -0.267890 0.299914	-0.230079 0.262701 0.937045	-0.129534 -0.000033 0.765804
19		52.581665 45.576813 0.353146	1.353722 -0.286667 0.292958	1.412375 1.594803 -0.594803	0.958471 -0.202968 0.200342	-0.152687 0.187817 0.968637	-0.123890 -0.001010 1.467603
20		52.553302 45.576732 0.431004	1.248807 -0.144275 0.160350	1.267299 1.606045 -0.606045	0.985408 -0.113855 0.126529	-0.111133 0.131253 0.945090	-0.124717 -0.000013 2.939258
21		55.437744 45.576732 0.631467	1.151564 -0.107118 0.086759	1.159783 1.345098 -0.345098	0.992913 -0.092460 0.074807	-0.067103 0.783750 0.994225	-0.105873 0.000014 5.469146
22		57.657056 45.576732 0.758877	1.101443 -0.113464 0.040674	1.109020 1.227709 -0.227709	0.994045 -0.102420 0.036709	-0.071933 0.047757 0.958348	-0.089066 0.000015 5.128668

BEST AVAILABLE COPY

PROGRAM JIMA
CASE NJ. NACA

DOUGLAS AIRCRAFT COMPANY
LCNG BEACH DIVISION
TUESDAY, NOV 30, 1976

NACA SWEPT WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL-SYM. P.KUTTA
UNIFORM CNSET FLOW = (0.585707E+00, 0.0 0.143106E+00)

ON - BODY		POINTS		FINAL		OUTPUT					
N	M	XO YO ZO	VX VY VZ	VT VISO CP	DCX DCY DCZ	NX NY NZ	SIG VN AREA				
1	23	60.155805 45.576787 0.755906	1.079902 -0.121326 0.005535	1.086710 1.180938 -0.180938	0.993735 -0.111645 0.005097	-0.002927 0.019474 0.999806	-0.079678 0.000015 4.872804				
24		62.352302 45.576787 0.755906	1.054834 -0.115364 -0.034754	1.061692 1.127191 -0.127191	0.993541 -0.108661 -0.032734	0.031566 -0.012578 0.999423	-0.076396 0.000014 4.649075				
25		64.446081 45.576787 0.755906	1.027301 -0.101651 -0.063210	1.034250 1.069674 -0.069674	0.993281 -0.098285 -0.061117	0.057854 -0.035854 0.997661	-0.075621 0.000014 4.445014				
26		66.444534 45.576787 0.755906	1.001915 -0.084749 -0.080116	1.008679 1.017433 -0.017433	0.993294 -0.094320 -0.079427	0.075365 -0.050617 0.995871	-0.076049 0.000014 4.254566				
27		68.355011 45.576787 0.755906	0.979033 -0.067501 -0.088103	0.935324 0.970863 0.029137	0.993636 -0.063506 -0.099415	0.085461 -0.058716 0.994610	-0.076769 0.000014 4.074959				
28		70.182807 45.576787 0.755906	0.961886 -0.058882 -0.087206	0.967429 0.935418 0.064082	0.994270 -0.057254 -0.090142	0.086721 -0.059616 0.994444	-0.075898 0.000014 3.904346				
29		71.511154 45.576787 0.755906	0.946126 -0.046083 -0.085578	0.951105 0.904601 0.095399	0.994765 -0.043453 -0.089977	0.087018 -0.059894 0.994405	-0.071717 -0.000039 1.887482				
30		72.367767 45.576787 0.755906	0.927117 -0.025123 -0.085377	0.926995 0.859319 0.140681	0.995386 -0.027101 -0.092047	0.090198 -0.062144 0.993983	-0.064498 -0.000035 1.951291				

THE FORCE COMPONENTS OF THIS STRIP ARE											
THE MOMENT COMPONENTS OF THIS STRIP ARE											

2	1	70.634796 43.386514 -0.340494	0.919066 0.085387 0.079212	0.926330 0.858087 0.141913	0.992159 0.020097 0.094497	0.090206 -0.061855 0.994001	0.077949 -0.000174 2.513225				

```

STREAMLINE NUMBER 1
IPRINT= 1 ISAVE= 1 ISTART= 1 ISTOP= 0 ISMODE= 0
IPANL= 0 DELTAS= 0.0200 XSI= 1.0932 YSI= 0.4258 ZSI= 0.0
DATA(1), I=1,21
IST S A(1) A(2) A(3) VSTAG
ICYCLE = 1 X, Y, Z = 72.369652 45.576431 -0.038452
ICYCLE = 2 X, Y, Z = 72.419434 45.179031 -0.013687
ICYCLE = 3 X, Y, Z = 72.342041 45.973770 -0.066086
1 0.023424 0.019767 0.0 0.957564
0.336011 0.333059 52.221207 45.577759 -0.287833 -0.727545
72.333652 45.576431 -0.033452 -0.996567 0.685791 0.071045
0.082031 0.083344 1.052539 0.425064 -0.086826 0.918457
0.995750 -0.036135 0.087967 0.060837 -0.994873 0.010986
DN, OK, D, RK = 0.253635 -0.026030 -0.037953 -0.148856
ICYCLE = 1 X, Y, Z = 71.961426 45.544418 -0.071182
ICYCLE = 2 X, Y, Z = 71.984375 45.145889 -0.044342
ICYCLE = 3 X, Y, Z = 71.936279 45.949875 -0.100861
50
DV = 0.320253 DOIT = 0.777651
VS(1) TO VS(9) 0.957510 0.306344 0.832545 52.186554 45.545745 -0.288265 -0.727657 -0.685946 -0.012061
2 0.023000 0.024110 0.037257 0.0 0.957510
0.358844 0.354418 45.545746 -0.288265 -0.727557 -0.012061
71.961426 45.544418 -0.071182 -0.996567 0.685791 0.938721
0.082031 0.083344 1.052539 0.425064 -0.086826 0.010986
0.995750 -0.036135 0.087967 0.060837 -0.994873 0.010986
DN, OK, D, RK = 0.253635 -0.026030 -0.037953 -0.148856
ICYCLE = 1 X, Y, Z = 71.561035 45.502975 -0.105453
ICYCLE = 2 X, Y, Z = 71.583008 45.094742 -0.076172
ICYCLE = 3 X, Y, Z = 71.515287 45.917358 -0.136261
DV = 0.322629 DOIT = 0.792695
VS(1) TO VS(9) 0.957439 0.307945 0.831868 52.141693 45.504227 -0.288825 -0.727804 -0.685787 -0.011994
3 0.023000 0.024999 0.054810 0.0 0.957439
0.357945 0.351168 45.504227 -0.288826 -0.727304 -0.011994
71.551035 45.512475 -0.105453 -0.997525 0.685791 0.956955
0.082031 0.083158 1.052539 0.425064 -0.086826 0.010986
0.995750 -0.036135 0.087967 0.060837 -0.994873 0.010986
DN, OK, D, RK = 0.253635 -0.026030 -0.037953 -0.148856
ICYCLE = 1 X, Y, Z = 71.149438 45.451309 -0.139359
ICYCLE = 2 X, Y, Z = 71.187500 45.034698 -0.108841
ICYCLE = 3 X, Y, Z = 71.093475 45.870453 -0.170486

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0.00000	0.026105	0.072603	0.0	0.957348	-0.685535	-0.011909
0.01000	52.065961	45.455530	-0.0	-0.727387	0.135986	0.963135
0.02000	-0.010356	-0.996629	-0.0	-0.972900	-0.036275	0.010636
0.03000	0.010356	0.996629	-1.001465	0.0		
0.04000	0.026105	0.072603	-0.997559	0.088021		
0.05000	0.042854	-0.035719	0.026215			
0.06000	0.058603	-0.035719	-0.172190			
0.07000	0.074352	45.389359	-0.141174			
0.08000	0.090101	44.967545	-0.204285			
0.09000	0.105850	45.810959				
0.10000	0.121599					
0.11000	0.137348					
0.12000	0.153097					
0.13000	0.168846					
0.14000	0.184595					
0.15000	0.200344					
0.16000	0.216093					
0.17000	0.231842					
0.18000	0.247591					
0.19000	0.263340					
0.20000	0.279089					
0.21000	0.294838					
0.22000	0.310587					
0.23000	0.326336					
0.24000	0.342085					
0.25000	0.357834					
0.26000	0.373583					
0.27000	0.389332					
0.28000	0.405081					
0.29000	0.420830					
0.30000	0.436579					
0.31000	0.452328					
0.32000	0.468077					
0.33000	0.483826					
0.34000	0.499575					
0.35000	0.515324					
0.36000	0.531073					
0.37000	0.546822					
0.38000	0.562571					
0.39000	0.578320					
0.40000	0.594069					
0.41000	0.609818					
0.42000	0.625567					
0.43000	0.641316					
0.44000	0.657065					
0.45000	0.672814					
0.46000	0.688563					
0.47000	0.704312					
0.48000	0.720061					
0.49000	0.735810					
0.50000	0.751559					
0.51000	0.767308					
0.52000	0.783057					
0.53000	0.798806					
0.54000	0.814555					
0.55000	0.830304					
0.56000	0.846053					
0.57000	0.861802					
0.58000	0.877551					
0.59000	0.893300					
0.60000	0.909049					
0.61000	0.924798					
0.62000	0.940547					
0.63000	0.956296					
0.64000	0.972045					
0.65000	0.987794					
0.66000	1.003543					
0.67000	1.019292					
0.68000	1.035041					
0.69000	1.050790					
0.70000	1.066539					
0.71000	1.082288					
0.72000	1.098037					
0.73000	1.113786					
0.74000	1.129535					
0.750						

OV = 0.79222 DOTT = 0.852537	VS(1) TO VS(9) 0.956621	0.824226	51.667377	45.064438	-0.295071	-0.729450	-0.684002	-0.011243
ICYLE = 1 X, Y, Z =	0.160000	0.034412	0.157299	0.956621	-0.684002	-0.011243		
ICYLE = 2 X, Y, Z =	0.322560	0.0300735	0.04438	-0.729450	0.28008	0.98881		
ICYLE = 3 X, Y, Z =	0.080195	1.605374	3.420333	0.990479	-0.284412	0.008881		
ON, DK, J, RK =	0.058138	0.085800	-0.059036	0.0				
ICYLE = 1 X, Y, Z =	0.160000	0.034412	0.157299	0.956621	-0.684002	-0.011243		
ICYLE = 2 X, Y, Z =	0.322560	0.0300735	0.04438	-0.729450	0.28008	0.98881		
ICYLE = 3 X, Y, Z =	0.080195	1.605374	3.420333	0.990479	-0.284412	0.008881		
ON, DK, J, RK =	0.058138	0.085800	-0.059036	0.0				
OV = 0.782413 DOTT = 0.855136	VS(1) TO VS(9) 0.956441	0.822560	51.568832	44.972321	-0.298424	-0.729809	-0.683613	-0.011080
ICYLE = 1 X, Y, Z =	0.160000	0.036384	0.174028	0.956441	-0.683613	-0.011080		
ICYLE = 2 X, Y, Z =	0.322560	0.032703	0.097162	-0.729809	0.214355	0.993652		
ICYLE = 3 X, Y, Z =	0.079346	1.667428	3.759624	0.993896	-0.214355	0.008377		
ON, DK, J, RK =	0.059082	0.085754	-0.059280	0.0				
ICYLE = 1 X, Y, Z =	0.160000	0.036384	0.174028	0.956441	-0.683613	-0.011080		
ICYLE = 2 X, Y, Z =	0.322560	0.032703	0.097162	-0.729809	0.214355	0.993652		
ICYLE = 3 X, Y, Z =	0.079346	1.667428	3.759624	0.993896	-0.214355	0.008377		
ON, DK, J, RK =	0.059082	0.085754	-0.059280	0.0				
OV = 0.765653 DOTT = 0.857658	VS(1) TO VS(9) 0.956254	0.820838	51.467209	44.877731	-0.297823	-0.730180	-0.683211	-0.010911
ICYLE = 1 X, Y, Z =	0.200000	0.038409	0.190601	0.956254	-0.683211	-0.010911		
ICYLE = 2 X, Y, Z =	0.322560	0.0364258	0.097406	-0.730180	0.216797	0.988291		
ICYLE = 3 X, Y, Z =	0.079422	1.791912	4.169279	0.994629	-0.216797	0.007523		
ON, DK, J, RK =	0.060791	0.085693	-0.059494	0.0				
ICYLE = 1 X, Y, Z =	0.200000	0.038409	0.190601	0.956254	-0.683211	-0.010911		
ICYLE = 2 X, Y, Z =	0.322560	0.0364258	0.097406	-0.730180	0.216797	0.988291		
ICYLE = 3 X, Y, Z =	0.079422	1.791912	4.169279	0.994629	-0.216797	0.007523		
ON, DK, J, RK =	0.060791	0.085693	-0.059494	0.0				

1207 3.1207 67.72323 3.233643 0.907498 DN, DK, J, RK =	0.219099 0.319991 44.711174 0.078514 -0.059814	0.043463 51.364136 -0.395944 1.887771 0.084747 3.347952	0.207157 44.781769 -0.997253 4.539919 -0.995850 -0.993408 -0.021664	0.958063 -0.730559 -0.998179 0.0 0.063843	-0.682931 -0.281436 -0.083420	-0.310739 -0.997356 0.007843
ICVCLF = 1 X, Y, Z =	67.285652	44.684616	-0.427185			
ICVCLF = 2 X, Y, Z =	67.373199	44.246231	-0.394379			
ICVCLF = 3 X, Y, Z =	67.187531	45.121735	-0.460266			
DV = 0.732170 DOTT = VS(1) TO VS(9) 0.955869 0.331610 0.817307	0.855886 0.331610	0.817307	51.260391	44.685196	-0.300691	-0.730942 -0.682385 -0.010564
13 2.331612 67.385652 0.955869 0.907787 DN, DK, J, RK =	0.219099 0.817307 44.711174 0.078514 -0.059814	0.043463 51.364136 -0.395944 1.887771 0.084747 3.347952	0.207157 44.781769 -0.997253 4.539919 -0.995850 -0.993408 -0.021664	0.958063 -0.730559 -0.998179 0.0 0.063843	-0.682931 -0.281436 -0.083420	-0.310739 -0.997356 0.007843
ICVCLF = 1 X, Y, Z =	66.848816	44.588577	-0.458023			
ICVCLF = 2 X, Y, Z =	66.933953	44.148834	-0.426117			
ICVCLF = 3 X, Y, Z =	66.747696	45.027069	-0.490753			
DV = 0.715412 DOTT = VS(1) TO VS(9) 0.955676 0.334465 0.815538	0.859142 0.334465	0.815538	51.157120	44.589005	-0.302131	-0.731325 -0.681970 -0.010389
14 3.334485 65.848816 3.229980 0.998138 DN, DK, J, RK =	0.259999 0.815538 44.589005 0.075316 -0.059814	0.043463 51.364136 -0.395944 1.887771 0.084747 3.347952	0.207157 44.781769 -0.997253 4.539919 -0.995850 -0.993408 -0.021664	0.958063 -0.730559 -0.998179 0.0 0.063843	-0.682931 -0.281436 -0.083420	-0.310739 -0.997356 0.007843
ICVCLF = 1 X, Y, Z =	66.408020	44.492401	-0.488754			
ICVCLF = 2 X, Y, Z =	66.496323	44.050552	-0.456879			
ICVCLF = 3 X, Y, Z =	66.308594	44.932022	-0.520264			
DV = 0.698365 DOTT = VS(1) TO VS(9) 0.955432 0.337362 0.813769	0.858885 0.337362	0.813769	51.053711	44.492561	-0.303374	-0.731709 -0.681554 -0.010214
15 3.337362 65.408020 3.232422 0.997695 DN, DK, J, RK =	0.279999 0.813769 44.492401 0.073776 -0.055176	0.043463 51.364136 -0.395944 1.887771 0.084747 3.347952	0.207157 44.781769 -0.997253 4.539919 -0.995850 -0.993408 -0.021664	0.958063 -0.730559 -0.998179 0.0 0.063843	-0.682931 -0.281436 -0.083420	-0.310739 -0.997356 0.007843
ICVCLF = 1 X, Y, Z =	65.965949	44.397354	-0.518600			
ICVCLF = 2 X, Y, Z =	66.052414	43.954651	-0.487915			
ICVCLF = 3 X, Y, Z =	65.866653	44.838593	-0.549149			
DV = 0.681875 DOTT = VS(1) TO VS(9) 0.955037 0.337937 0.813769	0.857937 0.337937	0.813769	51.053711	44.492561	-0.303374	-0.731709 -0.681554 -0.010214

1287 3.723220 67.723220 0.233543 0.007498 DN, DK, J, RK =	0.219009 0.319181 44.731174 0.074574 0.059314	0.042463 51.364136 -0.395444 1.687771 0.054747 J.347952	0.207157 44.781769 -0.947253 4.539919 -0.058289 -0.075543	0.099249 -0.582861 -0.995850 -0.993408 0.021664	0.956263 -0.730239 -0.998779 0.0 J.050843	-0.682801 -0.281436 -0.0083420	-0.710738 -0.997356 0.007843
ICVCLF = 1 X, Y, Z =	67.286652	44.684616	-0.427185	-0.427185			
ICVCLF = 2 X, Y, Z =	67.373199	44.246231	-0.394379	-0.394379			
ICVCLF = 3 X, Y, Z =	67.187531	45.121735	-0.440266	-0.440266			
DV = 0.732170 DQIT =	0.855686	0.817307					
VS(1) TO VS(9)	0.955869	0.331610	51.260391	44.585195	-0.300691	-0.730942	-0.682385
13 3.723220 67.723220 0.233543 0.007498 DN, DK, J, RK =	0.219009 0.319181 44.731174 0.074574 0.059314	0.042463 51.364136 -0.395444 1.687771 0.054747 J.347952	0.207157 44.781769 -0.947253 4.539919 -0.058289 -0.075543	0.099249 -0.582861 -0.995850 -0.993408 0.021664	0.956263 -0.730239 -0.998779 0.0 J.050843	-0.682801 -0.281436 -0.0083420	-0.710738 -0.997356 0.007843
ICVCLF = 1 X, Y, Z =	67.286652	44.684616	-0.427185	-0.427185			
ICVCLF = 2 X, Y, Z =	67.373199	44.246231	-0.394379	-0.394379			
ICVCLF = 3 X, Y, Z =	67.187531	45.121735	-0.440266	-0.440266			
DV = 0.715412 DQIT =	0.855676	0.815538					
VS(1) TO VS(9)	0.955676	0.334485	51.157120	44.589005	-0.302131	-0.731325	-0.681970
14 3.723220 67.723220 0.233543 0.007498 DN, DK, J, RK =	0.219009 0.319181 44.731174 0.074574 0.059314	0.042463 51.364136 -0.395444 1.687771 0.054747 J.347952	0.207157 44.781769 -0.947253 4.539919 -0.058289 -0.075543	0.099249 -0.582861 -0.995850 -0.993408 0.021664	0.956263 -0.730239 -0.998779 0.0 J.050843	-0.682801 -0.281436 -0.0083420	-0.710738 -0.997356 0.007843
ICVCLF = 1 X, Y, Z =	67.286652	44.684616	-0.427185	-0.427185			
ICVCLF = 2 X, Y, Z =	67.373199	44.246231	-0.394379	-0.394379			
ICVCLF = 3 X, Y, Z =	67.187531	45.121735	-0.440266	-0.440266			
DV = 0.598565 DQIT =	0.858885	0.813769					
VS(1) TO VS(9)	0.955492	0.337362	51.053711	44.492561	-0.303574	-0.731709	-0.681554
15 3.723220 67.723220 0.233543 0.007498 DN, DK, J, RK =	0.219009 0.319181 44.731174 0.074574 0.059314	0.042463 51.364136 -0.395444 1.687771 0.054747 J.347952	0.207157 44.781769 -0.947253 4.539919 -0.058289 -0.075543	0.099249 -0.582861 -0.995850 -0.993408 0.021664	0.956263 -0.730239 -0.998779 0.0 J.050843	-0.682801 -0.281436 -0.0083420	-0.710738 -0.997356 0.007843
ICVCLF = 1 X, Y, Z =	67.286652	44.684616	-0.427185	-0.427185			
ICVCLF = 2 X, Y, Z =	67.373199	44.246231	-0.394379	-0.394379			
ICVCLF = 3 X, Y, Z =	67.187531	45.121735	-0.440266	-0.440266			

3.293399	0.048685	0.273417	0.0	0.955292	-0.681163	-0.00042
3.813377	50.51690	44.997820	-0.0	-0.732088	0.216062	0.00633
45.37334	0.51690	-0.99710	-0.0	-0.002930	-0.077545	0.006485
3.229330	2.71852	-6.033398	-0.0	0.0		
0.654304	0.078400	-0.053329	0.072154			
DN, DK, D, RK =	0.361958	-0.077665				
ICVLE = 1 X, Y, Z =	65.525223	44.302887	-0.547806			
ICVLE = 2 X, Y, Z =	65.608765	43.858643	-0.518295			
ICVLE = 3 X, Y, Z =	65.426102	44.744888	-0.577240			
DN = 0.563383	0.857479	0.810301	50.850204	44.303115	-0.306413	-0.732465
VS(1) TO VS(9)	0.342596		0.0			-0.680734
17	0.050708	0.230020	-0.0	0.955102	-0.680734	-0.008870
3.342996	50.850204	44.303116	-0.306413	-0.732465	0.210205	1.008545
65.525223	-0.312867	-0.998444	-0.993408	-1.002930	-0.076233	0.004745
3.223633	2.360806	6.416003	-0.093652	0.0		
3.998672	0.069375	0.052174	0.029320			
DN, DK, D, RK =	-0.054288	-0.076446		0.075965		
ICVLE = 1 X, Y, Z =	65.080643	44.209244	-0.576447			
ICVLE = 2 X, Y, Z =	65.166229	43.763306	-0.547760			
ICVLE = 3 X, Y, Z =	64.984253	44.652161	-0.604279			
DN = 0.643264	0.856538	0.808600	50.749466	44.209320	-0.307814	-0.732838
VS(1) TO VS(9)	0.345761		0.0			-0.680330
18	0.053716	0.236652	-0.307814	0.954916	-0.680330	-0.009700
3.342996	50.749466	44.209320	-0.883105	-0.732358	0.205291	1.008348
65.080643	-0.312867	-0.998444	-0.996094	-1.005127	-0.072495	0.005173
3.223633	2.360806	6.416003	-0.093652	0.0		
3.998672	0.069375	0.052174	0.029320			
DN, DK, D, RK =	-0.054288	-0.076446		0.053830		
ICVLE = 1 X, Y, Z =	64.635468	44.116501	-0.604095			
ICVLE = 2 X, Y, Z =	64.718872	43.669418	-0.576782			
ICVLE = 3 X, Y, Z =	64.539551	44.560398	-0.630615			
DN = 0.631430	0.855467	0.806930	50.649811	44.116501	-0.309194	-0.733206
VS(1) TO VS(9)	0.348474		0.0			-0.679931
19	0.054702	0.233303	-0.309194	0.954733	-0.679931	-0.009533
3.342996	50.649811	44.116501	-0.683838	-0.733206	0.206543	1.007080
64.635468	-0.312867	-0.998444	-0.996332	-1.006104	-0.069526	0.005234
3.219238	2.552443	7.178964	-0.095972	0.0		
0.998655	0.067801	0.07058	0.023155	0.0		
DN, DK, D, RK =	0.365628	-0.075602		0.061373		
ICVLE = 1 X, Y, Z =	64.189484	44.024994	-0.630646			
ICVLE = 2 X, Y, Z =	64.271790	43.576920	-0.604767			
ICVLE = 3 X, Y, Z =	64.095795	44.470306	-0.655533			

20	0.379999	0.056663	0.339986	0.0	0.954554	-0.679539	-0.09368
21	0.805297	50.551361	44.024918	-0.0	-0.733553	0.203369	1.004578
66	0.324834	-0.633661	-0.958627	0.682861	-1.005371	-0.066556	
0.027775	2.643996	7.563389	-0.995850	-0.995850	0.0		
0.03779	0.063203	-0.042708	0.995758	0.021168	0.055885		
DN, DK, D, RK =	0.371425	-0.074246	0.021168				
ICYCLE = 1 X, Y, Z =	63.742676	43.936096	-0.656418				
ICYCLE = 2 X, Y, Z =	63.823212	43.486769	-0.631805				
ICYCLE = 3 X, Y, Z =	63.650925	44.382431	-0.679398				
DV =	0.597645	0.851457	0.803729	50.455780	43.936305	-0.311358	-0.733917
VS(1) TO VS(9)	0.954383	0.353672	0.356738	0.0	0.954383		-0.679161
21	0.359999	0.055566	0.356738	0.0	0.954383		
23	0.803729	50.455780	43.936096	-0.311858	-0.733917	-0.679161	-0.099209
63	0.324834	-0.633661	-0.958627	-0.682861	0.0	0.064911	0.003235
0.027775	2.643996	7.563389	-0.995850	-0.995850	0.0		
0.03779	0.063203	-0.042708	0.995758	-0.020837	0.054698		
DN, DK, D, RK =	0.371425	-0.074246	0.021168				
ICYCLE = 1 X, Y, Z =	63.294662	43.849121	-0.680893				
ICYCLE = 2 X, Y, Z =	63.373306	43.398758	-0.657944				
ICYCLE = 3 X, Y, Z =	63.204666	44.296417	-0.701996				
DV =	0.580670	0.849426	0.802215	50.362167	43.948369	-0.313129	-0.734256
VS(1) TO VS(9)	0.954217	0.356130	0.373547	0.0	0.954217		-0.009055
22	0.419999	0.060430	0.373547	0.0	0.954217		
23	0.803729	50.362167	43.849121	-0.313129	-0.734256	-0.673793	-0.009055
63	0.324834	-0.633661	-0.958627	-0.682861	0.0	0.064911	0.003235
0.027775	2.643996	7.563389	-0.995850	-0.995850	0.0		
0.03779	0.063203	-0.042708	0.995758	-0.020837	0.054698		
DN, DK, D, RK =	0.371425	-0.074246	0.021168				
ICYCLE = 1 X, Y, Z =	62.845566	43.763626	-0.704132				
ICYCLE = 2 X, Y, Z =	62.923218	43.312057	-0.682953				
ICYCLE = 3 X, Y, Z =	62.757477	44.211472	-0.723480				
DV =	0.563658	0.847860	0.800747	50.270020	43.763305	-0.314370	-0.734586
VS(1) TO VS(9)	0.954057	0.358513	0.390399	0.0	0.954057		-0.008905
23	0.439999	0.062263	0.390399	0.0	0.954057		
23	0.803729	50.270020	43.763626	-0.314370	-0.734586	-0.678435	-0.008905
62	0.324834	-0.633661	-0.958627	-0.682861	0.0	0.064911	0.003235
0.027775	2.643996	7.563389	-0.995850	-0.995850	0.0		
0.03779	0.063203	-0.042708	0.995758	-0.020837	0.054698		
DN, DK, D, RK =	0.371425	-0.074246	0.021168				
ICYCLE = 1 X, Y, Z =	62.396103	43.679749	-0.725952				
ICYCLE = 2 X, Y, Z =	62.471161	43.227676	-0.706833				
ICYCLE = 3 X, Y, Z =	62.307770	44.128464	-0.743290				

24 0.3508 62.3361J3 0.156213 0.009816 DN, DK, D, RK =	0.459968 0.453134 +3.579749 0.349729 -0.035438	0.064058 50.176779 -3.725952 2.039215 0.054228 0.378699	0.407891 43.699820 -0.099599 9.122714 -0.033112 -0.069155	0.0 -0.315573 -0.882678 -0.935453 -0.033112 0.024792	0.353333 -0.734907 -1.306012 0.0 0.064402	-0.679087 -0.184021 -0.053711	-0.308759 1.011459 0.002350
ICYLE = 1 X, Y, Z =	61.945313	43.597198	-0.746401				
ICYLE = 2 X, Y, Z =	62.020187	43.144180	-0.729063				
ICYLE = 3 X, Y, Z =	61.957971	44.046478	-0.761514				
DV = 0.529559 DINT =	0.844819	0.797966	50.090714	43.595893	-0.316745	-0.735220	-0.677748 -0.008617
VS(1) TO VS(9) 0.953754	0.363022	0.424195	0.0 -0.316745 -0.883746 -0.937116 -0.097620 0.023499	0.953754 -0.735220 -1.006653 0.0 0.060849	-0.677748 -0.185501 -0.049372	-0.008617 1.009369 0.001899	
25 0.363022 61.945313 3.195953 3.099729 DN, DK, D, RK =	0.479958 0.797966 43.527198 -0.045538 -0.011738	0.065827 50.090714 -0.746401 3.071814 0.051018 0.330020	0.424195 43.595893 -0.883746 9.511776 -0.097620 -0.068775	0.0 -0.316745 -0.883746 -0.937116 -0.097620 0.023499			
ICYLE = 1 X, Y, Z =	61.494186	43.514633	-0.765044				
ICYLE = 2 X, Y, Z =	61.568726	43.061096	-0.749942				
ICYLE = 3 X, Y, Z =	61.409059	43.984188	-0.777720				
DV = 0.512540 DINT =	0.845112	0.796629	50.001648	43.514252	-0.317903	-0.735528	-0.677413 -0.008476
VS(1) TO VS(9) 0.953609	0.365191	0.441069	0.0 -0.317903 -0.883136 -0.996155 -0.096689 0.020168	0.953609 -0.735528 -1.004608 0.0 0.052178	-0.677413 -0.181656 -0.045227	-0.008476 1.009537 0.001205	
26 0.365191 61.494186 3.192358 3.069961 DN, DK, D, RK =	0.459998 0.795629 43.514633 -0.041916 -0.027435	0.067595 50.001648 -0.765044 3.154391 0.045761 0.390582	0.441069 43.514252 -0.883136 9.912170 -0.025482 -0.067541	0.0 -0.317903 -0.883136 -0.996155 -0.096689 0.020168			
ICYLE = 1 X, Y, Z =	61.042084	43.433563	-0.782093				
ICYLE = 2 X, Y, Z =	61.114883	42.979675	-0.769109				
ICYLE = 3 X, Y, Z =	60.959122	43.883408	-0.792180				
DV = 0.495532 DINT =	0.843511	0.795348	49.914154	43.433197	-0.319024	-0.735827	-0.677089 -0.008341
VS(1) TO VS(9) 0.953471	0.367266	0.457969	0.0 -0.319024 -0.883960 -0.997833 -0.097498 0.019413	0.953471 -0.735827 -1.004333 0.0 0.050299	-0.677089 -0.180008 -0.039659	-0.008341 1.006500 0.001756	
27 0.367266 61.042084 3.189590 3.099881 DN, DK, D, RK =	0.519958 0.795348 43.433563 -0.033376 -0.021896	0.069331 49.914154 -0.782093 3.235431 0.040716 0.390295	0.457969 43.433197 -0.883960 10.308584 -0.097498 -0.065802	0.0 -0.319024 -0.883960 -0.997833 -0.097498 0.019413			
ICYLE = 1 X, Y, Z =	60.590515	43.354767	-0.797062				
ICYLE = 2 X, Y, Z =	60.661041	42.900787	-0.786687				
ICYLE = 3 X, Y, Z =	60.505109	43.834276	-0.804682				

28
 0.530659 0.071019 0.474906 0.0 0.320096 0.353340 -0.676779 -0.008211
 0.321064 43.354370 43.354370 -0.0 0.320096 -0.0 0.736113 -0.007590
 60.333737 43.354370 43.354370 -0.0 0.320096 -0.0 0.736113 -0.007590
 0.333730 3.14235 10.705226 -0.0 0.320096 -0.0 0.736113 -0.007590
 1.000000 0.333730 0.333730 -0.0 0.320096 -0.0 0.736113 -0.007590
 DN, DK, D, RK = 0.333730 0.333730 0.333730 0.0 0.320096 0.0 0.736113 0.000917
 0.333730 0.333730 0.333730 0.0 0.320096 0.0 0.736113 0.000917
 ICYCLE = 1 X, Y, Z = 60.138626 43.278030 -0.0 0.320096 -0.0 0.736113 0.000917
 ICYCLE = 2 X, Y, Z = 60.207581 42.823746 -0.0 0.320096 -0.0 0.736113 0.000917
 ICYCLE = 3 X, Y, Z = 60.056244 43.727661 -0.0 0.320096 -0.0 0.736113 0.000917
 0.054026

DV = 0.461349 DJIT = 0.839128
 VS(1) TO VS(9) 0.953218 0.371076 0.792994 49.745956 43.277634 -0.321121 -0.736386 -0.676483 -0.008087
 29
 0.559958 0.072662 0.491859 0.0 0.321121 0.953218 -0.676483 -0.008087
 0.371076 49.745956 49.745956 -0.0 0.321121 -0.0 0.736386 0.0005137
 60.133626 43.278030 43.278030 -0.0 0.321121 -0.0 0.736386 0.0005137
 0.180532 3.14235 11.105815 -0.0 0.321121 -0.0 0.736386 0.0005137
 1.000257 0.333730 0.333730 -0.0 0.321121 -0.0 0.736386 0.0005137
 DN, DK, D, RK = 0.333730 0.333730 0.333730 0.0 0.321121 0.0 0.736386 0.0005137
 ICYCLE = 1 X, Y, Z = 59.687256 43.201569 -0.0 0.321121 0.0 0.736386 0.0005137
 ICYCLE = 2 X, Y, Z = 59.756638 42.747833 -0.0 0.321121 -0.0 0.736386 0.0005137
 ICYCLE = 3 X, Y, Z = 59.604263 43.650330 -0.0 0.321121 -0.0 0.736386 0.0005137

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 DV = 0.444320 DJIT = 0.339197
 VS(1) TO VS(9) 0.353101 0.372353 0.791896 49.663116 43.201096 -0.322121 -0.736652 -0.676194 -0.007966
 30
 0.575958 0.074300 0.508781 0.0 0.322121 0.953101 -0.676194 -0.007966
 0.372353 49.663116 49.663116 -0.0 0.322121 -0.0 0.736652 0.000073
 59.687256 43.201569 43.201569 -0.0 0.322121 -0.0 0.736652 0.000073
 0.181326 3.14235 11.105815 -0.0 0.322121 -0.0 0.736652 0.000073
 1.000454 0.333730 0.333730 -0.0 0.322121 -0.0 0.736652 0.000073
 DN, DK, D, RK = 0.333730 0.333730 0.333730 0.0 0.322121 0.0 0.736652 0.000073
 ICYCLE = 1 X, Y, Z = 59.236389 43.123627 -0.0 0.322121 0.0 0.736652 0.000073
 ICYCLE = 2 X, Y, Z = 59.107007 42.670502 -0.0 0.322121 -0.0 0.736652 0.000073
 ICYCLE = 3 X, Y, Z = 59.153183 43.571533 -0.0 0.322121 -0.0 0.736652 0.000073

DV = 0.427443 DJIT = 0.841277
 VS(1) TO VS(9) 0.952988 0.374373 0.790829 49.579491 43.123154 -0.323114 -0.736916 -0.675906 -0.007846
 31
 0.599959 0.075971 0.525545 0.0 0.323114 0.952988 -0.675906 -0.007846
 0.374373 49.579491 49.579491 -0.0 0.323114 -0.0 0.736916 0.000259
 59.236389 43.123154 43.123154 -0.0 0.323114 -0.0 0.736916 0.000259
 0.181326 3.14235 11.105815 -0.0 0.323114 -0.0 0.736916 0.000259
 1.000462 0.333730 0.333730 -0.0 0.323114 -0.0 0.736916 0.000259
 DN, DK, D, RK = 0.333730 0.333730 0.333730 0.0 0.323114 0.0 0.736916 0.000259
 ICYCLE = 1 X, Y, Z = 58.786072 43.044952 -0.0 0.323114 0.0 0.736916 0.000259
 ICYCLE = 2 X, Y, Z = 58.857071 42.592880 -0.0 0.323114 -0.0 0.736916 0.000259
 ICYCLE = 3 X, Y, Z = 59.703552 43.492081 -0.0 0.323114 -0.0 0.736916 0.000259

[illegible]

36	0.659993	0.084256	0.608101	0.027546	0.952546	-0.674623	-0.738321	-0.674380	-0.007210
37	0.754773	49.156540	42.736359	-0.327546	-0.738321	-0.674623	-0.738321	-0.674380	-0.007210
38	42.736359	-0.327546	-0.000292	-0.882190	-0.738321	-0.674623	-0.738321	-0.674380	-0.007210
39	-0.327546	3.832275	13.678719	-0.947009	0.0	0.0007751	0.0007751	0.0007751	0.0007751
40	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
41	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
42	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
43	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
44	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
45	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
46	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
47	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
48	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
49	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
50	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
51	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
52	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
53	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
54	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
55	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
56	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
57	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
58	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
59	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751
60	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751	0.0007751

40 0.3341 55.22546 0.180328 0.999633 DN, DK, D, RK =	0.779997 0.733593 42.414932 0.013036 0.040573	0.001149 48.803696 -0.825241 4.254144 -0.024994 0.348956	0.671659 42.414673 -0.699664 15.426766 0.041061 -0.064056	0.0 -0.330848 0.683105 -0.998016 0.016762 -0.816055	0.352270 -0.738373 0.0 0.047245	-0.673670 0.176910 0.025513	-0.709916 0.956497 0.000580
ICYLE = 1 X, Y, Z =	54.787766	42.334030	-0.837646	-0.791183			
ICYLE = 2 X, Y, Z =	54.863815	41.895081					
ICYLE = 3 X, Y, Z =	54.703156	42.766464					
DV = 0.265014 DDTT = 0.848950 VS(1) TO VS(9) 0.387191 0.782941	0.392382 48.714783 -0.916055 4.235062 0.029931 0.343924	0.681197 42.333801 -0.809527 15.809109 0.044952 -0.063713	0.0 -0.331638 0.681458 -0.997375 -0.997360 0.017132	42.333901 0.352210 -0.739181 -0.347311 0.0 0.048979	-0.331638 -0.673443 0.174911 0.029190	-0.739181 -0.673443	-0.006821 0.950841 0.000763
41 0.387191 54.787766 0.179092 0.999481 DN, DK, D, RK =	0.799997 0.732341 42.334030 -0.020768 0.044152	0.392382 48.714783 -0.916055 4.235062 0.029931 0.343924	0.681197 42.333801 -0.809527 15.809109 0.044952 -0.063713	0.0 -0.331638 0.681458 -0.997375 -0.997360 0.017132	42.333901 0.352210 -0.739181 -0.347311 0.0 0.048979	-0.331638 -0.673443 0.174911 0.029190	-0.739181 -0.673443
ICYLE = 1 X, Y, Z =	54.352921	42.251892	-0.805435				
ICYLE = 2 X, Y, Z =	54.429840	41.815384	-0.829285				
ICYLE = 3 X, Y, Z =	54.265717	42.681580	-0.778259				
DV = 0.249627 DDTT = 0.851089 VS(1) TO VS(9) 0.398189 0.782311	0.392382 48.714783 -0.916055 4.235062 0.029931 0.343924	0.681197 42.333801 -0.809527 15.809109 0.044952 -0.063713	0.0 -0.331638 0.681458 -0.997375 -0.997360 0.017132	42.333901 0.352210 -0.739181 -0.347311 0.0 0.048979	-0.331638 -0.673443 0.174911 0.029190	-0.739181 -0.673443	-0.006821 0.950841 0.000763
42 0.387191 54.787766 0.179092 0.999481 DN, DK, D, RK =	0.799997 0.732341 42.334030 -0.020768 0.044152	0.392382 48.714783 -0.916055 4.235062 0.029931 0.343924	0.681197 42.333801 -0.809527 15.809109 0.044952 -0.063713	0.0 -0.331638 0.681458 -0.997375 -0.997360 0.017132	42.333901 0.352210 -0.739181 -0.347311 0.0 0.048979	-0.331638 -0.673443 0.174911 0.029190	-0.739181 -0.673443
ICYLE = 1 X, Y, Z =	53.921265	42.168809	-0.793533				
ICYLE = 2 X, Y, Z =	53.999680	41.732574	-0.819626				
ICYLE = 3 X, Y, Z =	53.830444	42.593521	-0.763977				
DV = 0.234536 DDTT = 0.855292 VS(1) TO VS(9) 0.399177 0.781686	0.392382 48.714783 -0.916055 4.235062 0.029931 0.343924	0.681197 42.333801 -0.809527 15.809109 0.044952 -0.063713	0.0 -0.331638 0.681458 -0.997375 -0.997360 0.017132	42.333901 0.352210 -0.739181 -0.347311 0.0 0.048979	-0.331638 -0.673443 0.174911 0.029190	-0.739181 -0.673443	-0.006821 0.950841 0.000763
43 0.387191 54.787766 0.179092 0.999481 DN, DK, D, RK =	0.799997 0.732341 42.334030 -0.020768 0.044152	0.392382 48.714783 -0.916055 4.235062 0.029931 0.343924	0.681197 42.333801 -0.809527 15.809109 0.044952 -0.063713	0.0 -0.331638 0.681458 -0.997375 -0.997360 0.017132	42.333901 0.352210 -0.739181 -0.347311 0.0 0.048979	-0.331638 -0.673443 0.174911 0.029190	-0.739181 -0.673443
ICYLE = 1 X, Y, Z =	53.492249	42.077621	-0.780441				
ICYLE = 2 X, Y, Z =	53.574524	41.646408	-0.808701				
ICYLE = 3 X, Y, Z =	53.397842	42.500977	-0.748627				

44	0.855997	0.058375	0.732244	0.0	0.352042	-0.672752	-	0.001434
3.3901	0.781059	48.432587	42.077499	-0.334053	-0.739816	0.196045	0.922089	
53.492244	42.077521	-0.780441	-0.999947	-0.683350	-0.925354	0.041809	0.001434	
0.193509	-0.022617	4.591505	16.929199	-0.999756	0.0			
0.889901	0.358044	-0.041499	0.057480	-0.998657	0.070893			
DN, DK, D, RK =	0.328367	-0.068714	-0.068714	0.023783				
ICYCLE = 1 X, Y, Z =	53.066589	41.985794	41.985794	-0.766159				
ICYCLE = 2 X, Y, Z =	53.152557	41.558014	41.558014	-0.796616				
ICYCLE = 3 X, Y, Z =	52.969589	42.405090	42.405090	-0.732361				
DN = 0.205374 DOIT = 0.864534	0.391137	0.780442	0.780442	48.331451	41.985764	-0.334887	-0.740033	-0.672514 -0.006437
VS(1) TO VS(9)	0.951990	0.107341	0.746615	0.0	0.351990	-0.672514	-0.006437	
45	0.376997	48.331451	41.985764	-0.334887	-0.740033	0.201416	0.912704	
3.39137	0.780442	-0.780442	-0.999947	-0.682892	0.0	0.046051	0.001485	
53.066589	41.985794	4.693274	17.292252	-0.999512	-0.915680			
0.204681	-0.032608	-0.045578	0.061829	-0.998428	0.0			
0.888749	0.063034	0.321553	-0.070383	0.022080	0.067077			
DN, DK, D, RK =	52.644150	41.891129	41.891129	-0.750900				
ICYCLE = 1 X, Y, Z =	52.733658	41.466797	41.466797	-0.783386				
ICYCLE = 2 X, Y, Z =	52.545563	42.305984	42.305984	-0.715271				
ICYCLE = 3 X, Y, Z =	52.545563	42.305984	42.305984	-0.715271				
DN = 0.191288 DOIT = 0.868581	0.392090	0.779835	0.779835	48.226974	41.891113	-0.335732	-0.740253	-0.672274 -0.006338
VS(1) TO VS(9)	0.951939	0.102370	0.760651	0.0	0.351939	-0.672274	-0.006338	
46	0.859937	0.102370	41.891113	-0.335732	-0.740253	0.206299	0.903015	
3.392090	0.773335	48.226974	-0.999947	-0.682373	0.0	0.050446	0.002243	
52.644150	41.891129	-0.780442	17.650353	-0.999779	0.0			
0.204681	-0.032608	4.778000	0.766330	-0.997589	0.059279			
0.889444	0.067123	-0.050064	-0.071391	0.019085				
DN, DK, D, RK =	0.313931	41.794479	41.794479	-0.734756				
ICYCLE = 1 X, Y, Z =	52.225601	41.374435	41.374435	-0.769104				
ICYCLE = 2 X, Y, Z =	52.317795	42.204605	42.204605	-0.697433				
ICYCLE = 3 X, Y, Z =	52.126251	42.204605	42.204605	-0.697433				
DN = 0.177512 DOIT = 0.871841	0.393013	0.779246	0.779246	48.120499	41.794693	-0.336573	-0.740472	-0.672035 -0.006239
VS(1) TO VS(9)	0.951890	0.104437	0.774378	0.0	0.351890	-0.672035	-0.006239	
47	0.919997	48.120499	41.794693	-0.336573	-0.740472	0.211670	0.891937	
3.393013	0.779246	-0.780442	-0.999947	-0.680835	0.0	0.055557	0.003220	
52.226651	41.794479	4.874492	18.002945	-0.998535	0.0			
0.213226	-0.036392	-0.054886	0.071320	-0.998826	0.051000			
0.887940	0.071834	0.334873	-0.071523	0.015971				
DN, DK, D, RK =	51.811386	41.695847	41.695847	-0.717880				
ICYCLE = 1 X, Y, Z =	51.905243	41.280075	41.280075	-0.753891				
ICYCLE = 2 X, Y, Z =	51.711884	42.100647	42.100647	-0.679031				
ICYCLE = 3 X, Y, Z =	51.711884	42.100647	42.100647	-0.679031				

49	0.93597	0.106552	0.787773	0.0	0.337429	0.951844	-0.671796	-0.740909	-0.671558	-0.006043
3.339	0.773571	48.011444	41.695999	-0.0	0.679199	-0.740692	0.214111			
51.421145	41.673447	-0.771780	-0.997681	0.0	0.996338	-0.883301	0.059814			
3.215195	-0.038132	4.973233	18.691774	-0.0	0.995026	0.0	0.003723			
0.997574	0.075912	-0.059433	0.076111	-0.0	0.013783	0.0				
DN, DK, D, RK =	0.235254	0.070733	-0.070733	0.0		0.045397				
ICycle = 1 X, Y, Z =	51.402145	41.595505	41.595505	-0.0	0.700241					
ICycle = 2 X, Y, Z =	51.497432	41.84692	41.84692	-0.0	0.737946					
ICycle = 3 X, Y, Z =	51.301132	41.995148	41.995148	-0.0	0.659866					
49	0.959997	0.108701	0.809851	0.0	0.338278	0.951802	-0.671558	-0.740909	-0.671558	-0.006043
3.394778	0.778115	47.900650	41.595795	-0.0	0.674909	-0.740909	0.218750			
51.402145	41.595505	-0.700241	-0.997681	0.0	0.996338	0.0	0.006043			
3.215195	-0.038132	5.073517	18.691437	-0.0	0.995026	0.0	0.873260			
0.997574	0.075912	-0.059433	0.076111	-0.0	0.013783	0.0	0.004684			
DN, DK, D, RK =	0.285308	0.070733	-0.070733	0.0		0.047134				
ICycle = 1 X, Y, Z =	50.598047	41.492645	41.492645	-0.0	0.682159					
ICycle = 2 X, Y, Z =	51.055154	41.086563	41.086563	-0.0	0.721420					
ICycle = 3 X, Y, Z =	50.895767	41.886703	41.886703	-0.0	0.640091					
50	0.975996	0.110904	0.812557	0.0	0.39135	0.951761	-0.671320	-0.741128	-0.671320	-0.005944
3.395622	0.777573	47.786880	41.492950	-0.0	0.674805	-0.741128	0.222412			
50.998047	41.492645	-0.682159	-0.998047	0.0	0.998047	0.0	0.005944			
3.221603	-0.038925	5.176391	19.025909	-0.0	0.991943	0.0	0.865814			
0.996429	0.082520	-0.069000	0.086151	-0.0	0.990311	0.0	0.006058			

DV = 0.001178 DJIT = 0.921616
 VS(1) TO VS(5) 0.351624 0.398757 0.775547 47.300964 41.054474 -0.342635 -0.005551
 54 1.053023 0.123304 0.860446 0.0 0.951624
 0.398757 0.775542 47.300964 41.054474 -0.342635 -0.670362 -0.005551
 49.334189 41.053140 -0.604111 0.0 0.742004 0.827240
 0.247803 -0.033738 5.515167 20.292910 -0.243512 0.010742
 0.993759 0.069354 -0.085752 0.108307 -0.091461
 DN, DK, D, RK = 0.233361 -0.072140 0.108721
 ICYCLE = 1 X, Y, Z = 49.055313 40.934372 -0.583466
 ICYCLE = 2 X, Y, Z = 49.164627 40.555481 -0.632004
 ICYCLE = 3 X, Y, Z = 48.927170 41.303268 -0.529297

DV = 0.080532 DJIT = 0.907984
 VS(1) TO VS(5) 0.351596 0.399496 0.775059 47.168320 40.935028 -0.343551 -0.005450
 55 1.079931 0.122865 0.871064 0.0 0.951596
 0.399496 0.775059 47.168320 40.935028 -0.343551 -0.670118 -0.005450
 49.334189 41.053140 -0.604111 0.0 0.742004 0.827240
 0.247803 -0.033738 5.515167 20.292910 -0.243512 0.010742
 0.993759 0.069354 -0.085752 0.108307 -0.091461
 DN, DK, D, RK = 0.233361 -0.072140 0.108721
 ICYCLE = 1 X, Y, Z = 49.055313 40.934372 -0.583466
 ICYCLE = 2 X, Y, Z = 49.164627 40.555481 -0.632004
 ICYCLE = 3 X, Y, Z = 48.927170 41.303268 -0.529297

DV = 0.070369 DJIT = 0.914972
 VS(1) TO VS(5) 0.351570 0.400224 0.774581 47.029236 40.939753 -0.344494 -0.005348
 55 1.099990 0.125551 0.831201 0.0 0.951570
 0.400224 0.774581 47.029236 40.939753 -0.344494 -0.669368 -0.005348
 49.334189 41.053140 -0.604111 0.0 0.742004 0.827240
 0.247803 -0.033738 5.515167 20.292910 -0.243512 0.010742
 0.993759 0.069354 -0.085752 0.108307 -0.091461
 DN, DK, D, RK = 0.233361 -0.072140 0.108721
 ICYCLE = 1 X, Y, Z = 48.307877 40.675705 -0.541733
 ICYCLE = 2 X, Y, Z = 48.431015 40.304886 -0.595276
 ICYCLE = 3 X, Y, Z = 48.146973 41.042450 -0.478119

DV = 0.060742 DJIT = 0.923350
 VS(1) TO VS(5) 0.351546 0.400949 0.774104 46.981241 40.576514 -0.345480 -0.005243
 57 1.115388 0.128406 0.890804 0.0 0.951546
 0.400949 0.774104 46.981241 40.576514 -0.345480 -0.669611 -0.005243
 49.334189 41.053140 -0.604111 0.0 0.742004 0.827240
 0.247803 -0.033738 5.515167 20.292910 -0.243512 0.010742
 0.993759 0.069354 -0.085752 0.108307 -0.091461
 DN, DK, D, RK = 0.233361 -0.072140 0.108721
 ICYCLE = 1 X, Y, Z = 47.937607 40.532776 -0.521011
 ICYCLE = 2 X, Y, Z = 43.070328 40.164734 -0.577484
 ICYCLE = 3 X, Y, Z = 47.754532 40.898178 -0.450195

OV = 0.051705	DIIT = 0.922593	46.722488	40.533752	-0.346519	-0.742935	-0.669344	-0.005134
VS(1) TO VS(9)	0.401674	0.773624	0.0	0.351526	0.0	0.0	0.0
59	0.131467	0.899821	0.0	0.772935	-0.669344	0.0	0.0
0.401674	46.722488	40.533752	-0.346519	-0.772935	0.0	0.0	0.0
47.037607	-0.521011	21.434067	-0.597559	0.0	0.0	0.0	0.0
0.310303	6.136628	21.434067	-0.597559	0.0	0.0	0.0	0.0
0.902889	0.111598	-0.131577	0.0	0.0	0.0	0.0	0.0
OV, DK, D, RK =	0.134217	-0.107993	0.0	0.0	0.0	0.0	0.0
ICVCL = 1 X, Y, Z =	47.569534	40.378540	-0.500534	0.290107	0.0	0.0	0.0
ICVCL = 2 X, Y, Z =	47.713745	40.012543	-0.560471	0.0	0.0	0.0	0.0
ICVCL = 3 X, Y, Z =	47.362946	40.739655	-0.420959	0.0	0.0	0.0	0.0
OV = 0.34326	DIIT = 0.942523	46.550934	40.379578	-0.347623	-0.743188	-0.669066	-0.005020
VS(1) TO VS(9)	0.402403	0.773139	0.0	0.351508	0.0	0.0	0.0
59	0.131473	0.908182	0.0	0.773188	-0.669066	0.0	0.0
0.402403	46.550934	40.379578	-0.347623	-0.773188	0.0	0.0	0.0
47.559534	-0.500534	21.434067	-0.597559	0.0	0.0	0.0	0.0
0.323754	6.295020	21.434067	-0.597559	0.0	0.0	0.0	0.0
0.902661	0.111711	-0.131577	0.0	0.0	0.0	0.0	0.0
OV, DK, D, RK =	0.134217	-0.107993	0.0	0.0	0.0	0.0	0.0
ICVCL = 1 X, Y, Z =	47.204971	40.211502	-0.480530	0.347379	0.0	0.0	0.0
ICVCL = 2 X, Y, Z =	47.360184	39.847687	-0.544342	0.0	0.0	0.0	0.0
ICVCL = 3 X, Y, Z =	46.978851	40.563095	-0.391861	0.0	0.0	0.0	0.0
OV = 0.35721	DIIT = 0.953029	46.365112	40.212616	-0.348790	-0.743451	-0.668778	-0.004903
VS(1) TO VS(9)	0.403134	0.772651	0.0	0.351494	0.0	0.0	0.0
60	0.133352	0.915773	0.0	0.772616	-0.668778	0.0	0.0
0.403134	46.365112	40.212616	-0.348790	-0.772616	0.0	0.0	0.0
47.204971	-0.480530	21.434067	-0.597559	0.0	0.0	0.0	0.0
0.356445	6.457548	21.434067	-0.597559	0.0	0.0	0.0	0.0
0.91974	0.124054	-0.131577	0.0	0.0	0.0	0.0	0.0
OV, DK, D, RK =	0.134217	-0.107993	0.0	0.0	0.0	0.0	0.0
ICVCL = 1 X, Y, Z =	46.846634	40.032776	-0.461151	0.399580	0.0	0.0	0.0
ICVCL = 2 X, Y, Z =	47.010986	39.671829	-0.529572	0.0	0.0	0.0	0.0
ICVCL = 3 X, Y, Z =	46.607712	40.369766	-0.364594	0.0	0.0	0.0	0.0
OV = 0.323928	DIIT = 0.962538	46.166122	40.033965	-0.350019	-0.743720	-0.668484	-0.004783
VS(1) TO VS(9)	0.403858	0.772166	0.0	0.351484	0.0	0.0	0.0
61	0.132182	0.922555	0.0	0.772166	-0.668484	0.0	0.0
0.403858	46.166122	40.033965	-0.350019	-0.772166	0.0	0.0	0.0
48.845634	-0.461151	21.434067	-0.597559	0.0	0.0	0.0	0.0
0.377197	6.636306	22.133563	-1.012939	0.0	0.0	0.0	0.0
0.900677	0.131714	-0.131577	0.0	0.0	0.0	0.0	0.0
OV, DK, D, RK =	0.134217	-0.107993	0.0	0.0	0.0	0.0	0.0
ICVCL = 1 X, Y, Z =	46.457849	39.844254	-0.442551	0.447854	0.0	0.0	0.0
ICVCL = 2 X, Y, Z =	46.668586	39.487961	-0.516144	0.0	0.0	0.0	0.0
ICVCL = 3 X, Y, Z =	46.						

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DOV =	0.213538	DOIT =	0.981301	45.513596	39.448792	-0.353897	-0.744458	-0.667629	-0.004436
VS(1)	VS(9)		0.405926	0.770772					
64	1.259373	0.154726	0.937945	0.0	0.951483	-0.667629	-0.004436		
3.405926	0.770772	45.513596	39.448792	-0.353897	-0.744499	0.426514	0.652588		
3.416748	-0.035319	-0.406237	-0.984268	-0.622598	0.657471	0.159470	0.027481		
3.984100	0.130664	7.221739	22.800354	-0.588281	0.3				
DN, DK, DR	0.196703	-0.156738	-0.141877	-0.974609	0.577839				
ICVCLF = 1	X, Y, Z =	45.519913	39.239716	-0.396881					
ICVCLF = 2	X, Y, Z =	45.709878	38.899124	-0.486191					
ICVCLF = 3	X, Y, Z =	45.270462	39.509918	-0.289422					

DT =	0.009580	DTT =	0.988261						
VS(1) T3 VS(9)	0.951490	0.406620	0.770307	45.281830	39.241180	-0.355232	-0.744732	-0.667372	-0.004332
NEXT STREAMLINE POINT EXCEEDS STAGNATION LIMIT									
65	1.273977	0.159176	0.941510	0.0	0.951490	-0.667372	-0.004332		
3.404620	0.770307	45.281830	39.241180	-0.355232	-0.744732	0.444580	0.637451		
45.215113	39.239116	-0.395881	-0.582300	-0.653691	0.637207	0.167953	0.031479		
3.432617	-0.26703	7.423422	22.974991	-0.985596	0.3				
0.992132	0.137256	-0.164017	0.189667	-0.970215					
DN. CK, D. RK =	3.170210	-0.143490		0.141072	3.592084				
LCPOINT =	517	VSPT =	65	ICND =	0	VT =	0.770307		

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LPPOINT = 517 VSP1 = 65 ICND = 0 VT = 0.770307

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END OF STREAMLINE ROUTINE.

LOFF	RAY	517	0	0	0	0	0	0
IFC	ARRAY	65	0	0	0	0	0	0
LDCD	ARRAY	0	0	0	0	0	0	0
IFD	ARRAY	0	0	0	0	0	0	0
LOSF	ARRAY	0	0	0	0	0	0	0

EIGHT STRIPS NACA SWEPT WING
 SET 1 STREAMLINE NO. 1
 FLAG1 = 1 FLAG2 = 2 FLAG3 = 0 FLAG4 = 0 FLAG5 = 0 NXY = 66 NTR = 10
 H1 = 3.01000
 EPS1 = 0.100000E-02
 VREF = 223.33000
 REREF = 0.670000E+07
 K = 1.14000
 SWANG = 0.0
 UE
 S
 P1 P3 P5

NX	X	S	UE	P1	P3	P5
1	0.0	0.0	0.17201E+03	0.0	0.10330E+01	0.0
2	0.14075E+00	0.14075E+00	0.17213E+03	0.20244E-01	0.10330E+01	-0.16033E+00
3	0.17224E+00	0.17224E+00	0.17308E+03	0.27330E-01	0.11943E+01	-0.18619E+00
4	0.20414E+00	0.20414E+00	0.17387E+03	0.37393E-01	0.13189E+01	-0.20864E+00
5	0.23655E+00	0.23655E+00	0.17514E+03	0.54155E-01	0.14338E+01	-0.24469E+00
6	0.26973E+00	0.26973E+00	0.17650E+03	0.75703E-01	0.14436E+01	-0.28978E+00
7	0.30311E+00	0.30311E+00	0.17844E+03	0.10444E+00	0.14535E+01	-0.32109E+00
8	0.33653E+00	0.33653E+00	0.18061E+03	0.13439E+00	0.14031E+01	-0.35329E+00
9	0.36990E+00	0.36990E+00	0.18225E+03	0.16047E+00	0.12877E+01	-0.33729E+00
10	0.40302E+00	0.40302E+00	0.18589E+03	0.16972E+00	0.11173E+01	-0.32030E+00
11	0.43603E+00	0.43603E+00	0.18843E+03	0.17104E+00	0.94133E+00	-0.29722E+00
12	0.46903E+00	0.46903E+00	0.19077E+03	0.17096E+00	0.76348E+00	-0.25345E+00
13	0.50213E+00	0.50213E+00	0.19303E+03	0.15905E+00	0.65517E+00	-0.23593E+00
14	0.53555E+00	0.53555E+00	0.19493E+03	0.14796E+00	0.52143E+00	-0.21341E+00
15	0.56924E+00	0.56924E+00	0.19664E+03	0.15192E+00	0.47851E+00	-0.18017E+00
16	0.60330E+00	0.60330E+00	0.19839E+03	0.13882E+00	0.43231E+00	-0.16734E+00
17	0.63770E+00	0.63770E+00	0.19976E+03	0.12960E+00	0.35954E+00	-0.16873E+00
18	0.67248E+00	0.67248E+00	0.20120E+03	0.15747E+00	0.38335E+00	-0.17204E+00
19	0.70752E+00	0.70752E+00	0.20306E+03	0.18468E+00	0.38549E+00	-0.13357E+00
20	0.74313E+00	0.74313E+00	0.20494E+03	0.20650E+00	0.45480E+00	-0.14202E+00
21	0.77895E+00	0.77895E+00	0.20712E+03	0.21206E+00	0.55411E+00	-0.13976E+00
22	0.81505E+00	0.81505E+00	0.20900E+03	0.19661E+00	0.65536E+00	-0.17931E+00
23	0.85136E+00	0.85136E+00	0.21077E+03	0.20307E+00	0.72427E+00	-0.17424E+00
24	0.88780E+00	0.88780E+00	0.21266E+03	0.19590E+00	0.75511E+00	-0.25171E+00
25	0.92457E+00	0.92457E+00	0.21420E+03	0.19449E+00	0.65344E+00	-0.19873E+00
26	0.96146E+00	0.96146E+00	0.21597E+03	0.19155E+00	0.56539E+00	-0.99617E-01

28	0.10353E+01	0.10358E+01	0.21915E+03	0.19258E+00	0.62770E+00	-0.37029E-01
29	0.10733E+01	0.10738E+01	0.22043E+03	0.14924E+00	0.75538E+00	-0.17257E-01
30	0.11103E+01	0.11108E+01	0.22145E+03	0.13926E+00	0.82251E+00	-0.89896E-01
31	0.11483E+01	0.11488E+01	0.22252E+03	0.12044E+00	0.88500E+00	-0.15987E+00
32	0.11861E+01	0.11866E+01	0.22321E+03	0.11612E+00	0.76522E+00	-0.96072E-01
33	0.12240E+01	0.12245E+01	0.22417E+03	0.15088E+00	0.75737E+00	0.20283E-01
34	0.12619E+01	0.12619E+01	0.22530E+03	0.13677E+00	0.78736E+00	0.95910E-01
35	0.12999E+01	0.12999E+01	0.22602E+03	0.13662E+00	0.90738E+00	0.34212E-01
36	0.13380E+01	0.13380E+01	0.22711E+03	0.12980E+00	0.10122E+01	-0.65121E-01
37	0.13761E+01	0.13761E+01	0.22770E+03	0.80301E-01	0.11132E+01	-0.12622E+00
38	0.14143E+01	0.14143E+01	0.22812E+03	0.90059E-01	0.11213E+01	0.11283E-01
39	0.14525E+01	0.14525E+01	0.22881E+03	0.61603E-01	0.94158E+00	0.17283E+00
40	0.14907E+01	0.14907E+01	0.22986E+03	0.73625E-01	0.89979E+00	0.18026E+00
41	0.15290E+01	0.15290E+01	0.22968E+03	0.83414E-01	0.95739E+00	0.14114E+00
42	0.15673E+01	0.15673E+01	0.22982E+03	0.58958E-01	0.11444E+01	-0.25043E-02
43	0.16055E+01	0.16055E+01	0.23034E+03	0.42075E-01	0.12408E+01	0.13898E+00
44	0.16437E+01	0.16437E+01	0.23029E+03	-0.14759E-02	0.10192E+01	0.15241E+00
45	0.16818E+01	0.16818E+01	0.23032E+03	0.26555E-01	0.11186E+01	0.15682E+00
46	0.17199E+01	0.17199E+01	0.23056E+03	0.33917E-01	0.11249E+01	0.20672E+00
47	0.17579E+01	0.17579E+01	0.23067E+03	0.31258E-02	0.11799E+01	0.27680E+00
48	0.17959E+01	0.17959E+01	0.23060E+03	-0.59495E-02	0.13226E+01	0.13799E+00
49	0.18339E+01	0.18339E+01	0.23061E+03	0.62974E-01	0.11346E+01	0.10153E+00
50	0.18718E+01	0.18718E+01	0.23120E+03	0.43090E-02	0.17363E+01	0.15084E+00
51	0.19095E+01	0.19095E+01	0.23066E+03	-0.72784E-01	0.16536E+01	0.75039E-01
52	0.19472E+01	0.19472E+01	0.23053E+03	0.29004E-01	0.12972E+01	0.12787E+00
53	0.19849E+01	0.19849E+01	0.23091E+03	-0.10862E-01	0.18772E+01	0.57192E-01
54	0.20223E+01	0.20223E+01	0.23044E+03	-0.11528E+00	0.15137E+01	0.90112E-01
55	0.20597E+01	0.20597E+01	0.22993E+03	-0.12145E+00	0.15338E+01	-0.57923E-01
56	0.20969E+01	0.20969E+01	0.22943E+03	-0.20265E+00	0.19596E+01	-0.10756E+00
57	0.21339E+01	0.21339E+01	0.22829E+03	-0.29639E+00	0.18807E+01	-0.25675E+00
58	0.21703E+01	0.21703E+01	0.22709E+03	-0.30933E+00	0.17032E+01	-0.27063E+00
59	0.22073E+01	0.22073E+01	0.22591E+03	-0.44504E+00	0.15222E+01	-0.50315E+00
60	0.22437E+01	0.22437E+01	0.22378E+03	0.40564E+00	0.14316E+01	-0.85370E+00

62	0.23160E+01	0.22101E+03	-0.67261E+00	0.72154E+01	-0.12629E+01
63	0.23514E+01	0.21840E+03	0.75863E+00	0.24837E+01	-0.14839E+01
64	0.23862E+01	0.21606E+03	-0.10885E+01	0.32296E+01	-0.15126E+01
65	0.24158E+01	0.21173E+03	-0.15452E+01	0.34972E+00	-0.17408E+01
66	0.24540E+01	0.20688E+03	-0.16824E+01	-0.43835E+01	-0.19781E+01

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[illegible]

PROGRAM	JINVA	DOUGLAS	AIRCRAFT	COMPANY	PAGE
CASE NO. NACA		LONG	BEACH	DIVISION	
		FRIDAY,	MAR 4,	1977	
		NACA	SWEPT WING,	8 STIPS,	A-8.22, 30 SOURCE, 1 WAKE, 1 PL.SYM.
					ONE

NACA SWEEP WING, 8 STRIPS, $A=8.22$, 30 SOURCE, 1 WAKE, 1 PL-SYM. ONE

[illegible]

COMPONENTS OF THE UNIFORM ONSET FLOWS

(1) 0.989707, 0.0, 0.143106

OTHER INPUT INFORMATION WILL BE WRITTEN ELSEWHERE IN THE OUTPUT.

PROGRAM JIWA
CASE NO. NICA

DOUGLAS AIRCRAFT COMPANY
LONG BEACH DIVISION
FRIDAY, MAR 4, 1977

PAGE 2.

NACA SWEPT WING, 8 STIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL-SYM. ONE

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BEGIN THE SUBROUTINE INPUT. TIME IS 0.023 SEC.

BEGIN THE FORMATION OF ELEMENTS. TIME IS 0.099 SEC.

PROGRAM JIMA DOUGLAS AIRCRAFT COMPANY
CASE NO. NACA LONG BEACH, MAR 4, 1977
NACA SWEEP WING, 8 STRIPS, A=9.22, 30 SOURCE, 1 PL. SYM. ONE

N	M	X	Y	Z	X	Y	Z	X	Y	Z	NX	NY	NZ	X0	Y0	Z0	TYPE OF ELEMENT	LIFT
1	1	73.540233	72.713735	71.185577	72.053513	0.081502	72.370789	3.5148E-05										
		46.668198	44.498032	44.498032	44.498032	-0.054681	45.574738	3.2037E+00										
		-0.036140	-0.104620	-0.110410	-0.039240	-0.995172	-0.072470	1.8513E+00										
2	2	72.718735	71.872849	70.300583	71.195577	0.081509	71.513565	3.4060E-05										
		46.668198	44.498032	44.498032	44.498032	-0.054681	45.574738	3.2037E+00										
		-0.036140	-0.104620	-0.110410	-0.039240	-0.995172	-0.072470	1.8513E+00										
3	3	71.872849	70.300583	69.470444	70.300583	0.084630	70.185806	2.4015E-05										
		46.668198	44.498032	44.498032	44.498032	-0.054681	45.574738	3.2037E+00										
		-0.036140	-0.104620	-0.110410	-0.039240	-0.995172	-0.072470	1.8513E+00										
4	4	70.123810	68.297974	66.560074	68.470444	0.083837	68.256659	2.3186E-05										
		46.668198	44.498032	44.498032	44.498032	-0.054681	45.574738	3.2037E+00										
		-0.036140	-0.104620	-0.110410	-0.039240	-0.995172	-0.072470	1.8513E+00										
5	5	68.297974	66.560074	64.562836	66.560074	0.074213	66.445786	7.0870E-05										
		46.668198	44.498032	44.498032	44.498032	-0.054681	45.574738	3.2037E+00										
		-0.036140	-0.104620	-0.110410	-0.039240	-0.995172	-0.072470	1.8513E+00										
6	6	66.560074	64.562836	62.472443	64.562836	0.056776	64.4466930	8.9645E-05										
		46.668198	44.498032	44.498032	44.498032	-0.054681	45.574738	3.2037E+00										
		-0.036140	-0.104620	-0.110410	-0.039240	-0.995172	-0.072470	1.8513E+00										
7	7	64.562836	62.472443	60.282272	62.472443	0.030596	62.353668	6.9372E-05										
		46.668198	44.498032	44.498032	44.498032	-0.054681	45.574738	3.2037E+00										
		-0.036140	-0.104620	-0.110410	-0.039240	-0.995172	-0.072470	1.8513E+00										
8	8	62.472443	60.282272	57.985003	60.282272	0.0203904	60.159760	4.2658E-05										
		46.668198	44.498032	44.498032	44.498032	-0.054681	45.574738	3.2037E+00										
		-0.036140	-0.104620	-0.110410	-0.039240	-0.995172	-0.072470	1.8513E+00										
9	9	60.282272	57.985003	55.572815	57.985003	0.0033193	57.856781	4.6231E-06										
		46.668198	44.498032	44.498032	44.498032	-0.054681	45.574738	3.2037E+00										
		-0.036140	-0.104620	-0.110410	-0.039240	-0.995172	-0.072470	1.8513E+00										
10	10	57.985003	55.572815	53.033498	55.572815	-0.068656	55.437408	1.8835E-05										
		46.668198	44.498032	44.498032	44.498032	-0.054681	45.574738	3.2037E+00										
		-0.036140	-0.104620	-0.110410	-0.039240	-0.995172	-0.072470	1.8513E+00										
11	11	55.572815	53.033498	51.720642	53.033498	-0.113772	53.553650	3.1263E-05										
		46.668198	44.498032	44.498032	44.498032	-0.054681	45.574738	3.2037E+00										
		-0.036140	-0.104620	-0.110410	-0.039240	-0.995172	-0.072470	1.8513E+00										
12	12	53.033498	51.720642	51.051102	51.720642	-0.165237	52.581333	2.0701E-05										
		46.668198	44.498032	44.498032	44.498032	-0.054681	45.574738	3.2037E+00										
		-0.036140	-0.104620	-0.110410	-0.039240	-0.995172	-0.072470	1.8513E+00										

DOUGLAS AIRCRAFT COMPANY
LONG BEACH DIVISION
FRIDAY, MAR 4, 1977
NACA SWEPT WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL.SYM.

PROGRAM JIMA
CASE NO. NACA

N	M	X Y Z	X Y Z	X Y Z	X Y Z	NX NY NZ	XO YO ZO	D Y A	TYPE OF ELEMENT
1	13	53.476013 46.669403 -0.289150	53.151306 46.668868 -0.203570	50.715271 44.499161 -0.212800	51.051102 44.499588 -0.233230	-0.232663 0.266078 -0.935453	52.091583 45.578140 -0.255223	8.16588E-06 3.5123E+00 7.6478E-01	LIFT
14		53.151306 46.668868 -0.203570	52.955795 46.669510 -0.139140	50.506866 44.499680 -0.144670	50.715271 44.499161 -0.212800	-0.315534 0.358787 -0.878470	51.819290 45.572739 -0.177842	2.7247E-05 3.4209E+00 5.0046E-01	
15		52.955795 46.669510 -0.139140	52.824539 46.670425 -0.000010	50.369522 44.500458 -0.000010	50.506866 44.499680 -0.144670	-0.559424 0.632953 -0.535179	51.654800 45.576706 -0.070720	3.8747E-05 3.3781E+00 5.4843E-01	
16		52.824539 46.670425 -0.000010	52.955063 46.670334 0.140130	50.506271 44.500351 0.146280	50.369522 44.500458 -0.000010	-0.563258 0.637181 0.526061	51.654724 45.577316 0.071609	7.2718E-05 3.2765E+00 5.5173E-01	
17		52.955063 46.670334 0.140130	53.150070 46.670273 0.212580	50.714294 44.500259 0.222970	50.506271 44.500351 0.146280	-0.322756 0.366581 0.872610	51.818466 45.573776 0.180534	1.2644E-04 3.4209E+00 5.0133E-01	
18		53.150070 46.670273 0.212580	53.475174 46.670364 0.263240	51.050461 44.500336 0.306330	50.714294 44.500259 0.222970	-0.232183 0.265088 0.935853	52.090698 45.579239 0.258813	1.3104E-05 3.5124E+00 7.6647E-01	
19		53.475174 46.670364 0.263240	54.115311 46.671609 0.403090	51.720154 44.500549 0.421140	51.050461 44.500336 0.306330	-0.165991 0.191283 0.967397	52.581192 45.577286 0.356008	2.9009E-05 3.7567E+00 1.4689E+00	
20		54.115311 46.670609 0.403090	55.374832 46.670837 0.549870	53.038086 44.500793 0.574370	51.720154 44.500549 0.421140	-0.114589 0.134583 0.984255	53.553146 45.577484 0.487198	8.6069E-05 4.2524E+00 2.8407E+00	
21		55.374832 46.670837 0.549870	57.797119 46.670337 0.718540	55.572525 44.501819 0.750800	53.038086 44.500793 0.574370	-0.069109 0.085725 0.999313	55.437012 45.577621 0.648502	1.1683E-05 5.2324E+00 5.4111E+00	
22		57.797119 46.670337 0.718540	60.103561 46.670563 0.796880	57.985870 44.500549 0.832880	55.572525 44.500809 0.750800	-0.033922 0.049639 0.998191	57.856552 45.577484 0.774903	2.7478E-05 5.0240E+00 5.1309E+00	
23		60.103561 46.670563 0.796880	62.208538 46.670013 0.807780	60.282440 44.507015 0.844340	57.985870 44.500549 0.832880	-0.004972 0.021450 0.999758	60.159790 45.577087 0.820607	1.3694E-05 4.8277E+00 4.8754E+00	
24		62.208538 46.670013 0.807780	64.392136 46.665266 0.766680	62.473053 44.499268 0.780000	60.282440 44.500015 0.844340	-0.029164 0.010253 0.999522	62.354095 45.576431 0.764937	2.9313E-06 4.6481E+00 4.6521E+00	

DOUGLAS AIRCRAFT COMPANY
LONG BEACH, MAR 4, 1977
NACA SWEPT WING, 8 STRIPS, A=22, 30 SOURCE, 1 WAKE, 1 PL-SYM. ONE

NACA SHEET WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL.SYM. ONE																	
N	M	X			Y			Z			NX			XO			TYPE OF ELEMENT
		X	Y	Z	X	Y	Z	X	Y	Z	NX	NY	NZ	XO	YO	ZO	
1	25	64.392136	66.390518	64.563950	62.473053	0.055130	0.000000	0.055130	64.447830	1.6503E-06	LIFT						
		46.669266	46.668503	44.498474	44.498474	-0.033241	-0.000000	-0.033241	45.575884	4.4803E+00							
		0.746690	0.696260	0.664880	0.780420	0.997926	0.000000	0.997926	0.707177	4.4476E+00							
		66.390518	68.298744	66.561722	64.563950	0.072285	0.000000	0.072285	66.447235	3.5502E-06							
2	26	46.667786	46.667786	44.497757	44.498474	-0.047702	-0.000000	-0.047702	45.574905	4.3232E+00							
		0.636260	0.497690	0.519900	0.664880	0.996243	0.000000	0.996243	0.579778	4.2564E+00							
		68.299744	70.125977	68.472458	66.561722	0.082183	0.000000	0.082183	68.358566	5.4836E-05							
		46.667786	46.667267	44.497223	44.497757	-0.055688	-0.000000	-0.055688	45.574310	4.1762E+00							
3	27	0.487690	0.346940	0.361950	0.451990	0.995060	0.000000	0.995060	0.431690	4.0757E+00							
		70.125977	71.875200	70.302841	68.472458	0.083066	0.000000	0.083066	70.180034	1.3471E-04							
		46.667267	46.666840	44.496911	44.497223	-0.055636	-0.000000	-0.055636	45.573922	4.0383E+00							
		0.346940	0.201140	0.208840	0.361950	0.994939	0.000000	0.994939	0.279760	3.9044E+00							
4	28	71.875200	72.721451	71.188126	70.302841	0.078403	0.000000	0.078403	71.516068	1.4534E-05							
		46.666840	46.666321	44.496277	44.496911	-0.053293	-0.000000	-0.053293	45.573364	3.2499E+00							
		0.201140	0.134500	0.139060	0.208840	0.995456	0.000000	0.995456	0.170908	1.8980E+00							
		72.721451	73.551239	72.056351	71.188126	0.078404	0.000000	0.078404	72.373566	1.5102E-05							
5	30	46.666321	46.665802	44.495743	44.496277	-0.053321	-0.000000	-0.053321	45.572830	3.2087E+00							
		0.134500	0.069150	0.070620	0.139060	0.995456	0.000000	0.995456	0.103344	1.8516E+00							
		74.390035	74.390035	72.923553	72.056351	0.0	0.000000	0.0	73.222214	3.4692E-08	WAKE						
		46.665802	46.665802	44.495743	44.495743	0.000677	0.000000	0.000677	45.572511	3.1794E+00							
6	31	0.069150	0.069150	0.070620	0.070620	1.000000	0.000000	1.000000	0.069890	1.8402E+00							
		72.923553	74.390035	72.923553	72.923553	0.000677	0.000000	0.000677	73.222214	3.4692E-08							
		46.665802	46.665802	44.495743	44.495743	0.000677	0.000000	0.000677	45.572511	3.1794E+00							
		0.069150	0.069150	0.070620	0.070620	1.000000	0.000000	1.000000	0.069890	1.8402E+00							
7	1	72.053513	71.185577	69.216279	70.134262	0.001374	0.000000	0.001374	70.638321	9.5632E-05	LIFT						
		44.497711	44.498032	41.697556	41.697199	-0.052762	-0.000000	-0.052762	43.084534	3.9872E+00							
		-0.039240	-0.110410	-0.122770	-0.122770	-0.995286	0.000000	-0.995286	-0.080126	2.5132E+00							
		71.185577	70.300583	68.280228	69.216279	0.081376	0.000000	0.081376	69.736328	9.5621E-05							
8	2	44.498032	44.498367	41.697937	41.697556	-0.052900	-0.000000	-0.052900	43.084869	4.0360E+00							
		-0.110410	-0.122980	-0.122770	-0.122770	-0.995279	0.000000	-0.995279	-0.153889	2.5627E+00							
		70.300583	68.470444	66.344467	68.280228	0.084463	0.000000	0.084463	68.339218	1.8632E-04							
		44.498367	44.498566	41.698242	41.697937	-0.055331	-0.000000	-0.055331	43.085190	4.8501E+00							
9	3	-0.122980	-0.122980	-0.122770	-0.122770	-0.994889	0.000000	-0.994889	-0.271085	5.3006E+00							
		68.470444	66.560074	64.323776	66.344467	0.083591	0.000000	0.083591	66.414474	2.1869E-04							
		44.498566	44.498871	41.698353	41.698242	-0.054058	-0.000000	-0.054058	43.085680	5.0072E+00							
		-0.122980	-0.122980	-0.122770	-0.122770	-0.994889	0.000000	-0.994889	-0.433631	5.5325E+00							
10	4	68.470444	66.560074	64.323776	66.344467	0.083591	0.000000	0.083591	66.414474	2.1869E-04							
		44.498566	44.498871	41.698353	41.698242	-0.054058	-0.000000	-0.054058	43.085680	5.0072E+00							
		-0.122980	-0.122980	-0.122770	-0.122770	-0.994889	0.000000	-0.994889	-0.433631	5.5325E+00							
		68.470444	66.560074	64.323776	66.344467	0.083591	0.000000	0.083591	66.414474	2.1869E-04							
11	5	44.498871	44.499207	41.698353	41.698242	-0.054058	-0.000000	-0.054058	43.085680	5.0072E+00							
		-0.122980	-0.122980	-0.122770	-0.122770	-0.994889	0.000000	-0.994889	-0.433631	5.5325E+00							
		68.470444	66.560074	64.323776	66.344467	0.083591	0.000000	0.083591	66.414474	2.1869E-04							
		44.498871	44.499207	41.698353	41.698242	-0.054058	-0.000000	-0.054058	43.085680	5.0072E+00							

PAGE 26.

PROGRAM JIHA
CASE NO. NACA
DOUGLAS AIRCRAFT COMPANY
LONG BEACH DIVISION
FRIDAY, MAR 4, 1977
NACA SWEPT WING, 8 STRIPS, A=3.22, 30 SOURCE, 1 WAKE, 1 PL-SYM. ONE
UNIFORM ONSET FLOW = (0.989707E+00, 0.0 , 0.143106E+00)

FINAL OUTPUT FOR THE FOLLOWING ANGLE OF ATTACK

(0.989707, 0.0 , 0.143106)

DOUGLAS AIRCRAFT COMPANY
 LONG BEACH, CALIF. 4, 1977
 NACA SWEPT WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL-SYM. ONE
 UNIFORM ONSET FLOW = (0.989707E+00, 0.0 , 0.143106E+00)

N	M	ON - BODY			POINTS			FINAL			OUTPUT			SIG		
		VX	VY	VZ	VT	VSQ	CP	DCX	DCY	DCZ	NX	NY	NZ	SVN	AREA	
1	1	72.370789	0.927096	0.936872	0.877729	0.123479	0.074255	0.989565	0.081502	0.037847	0.081502	0.037847	0.037847	0.037847	0.037847	
		45.574738	0.115684	0.877729	0.123479	0.074255		0.123479	-0.054681	0.000003	-0.054681	0.000003	0.000003	0.000003	1.851255	
		-0.072470	0.069567	0.122271				0.074255	-0.995172		-0.995172					
2		71.513565	0.969444	0.932287	0.877729	0.123479	0.074255	0.986926	0.081509	0.054783	0.081509	0.054783	0.054783	0.054783	0.054783	
		45.575089	0.141180	0.877729	0.123479	0.074255		0.143726	-0.054623	0.000005	-0.054623	0.000005	0.000005	0.000005	1.337727	
		-0.142655	0.071647	0.035113				0.072939	-0.995175		-0.995175					
3		70.185906	0.989065	1.011964	0.877729	0.123479	0.074255	0.977372	0.084630	0.064063	0.084630	0.064063	0.064063	0.064063	0.064063	
		45.575333	0.201360	1.024071	0.877729	0.123479	0.074255	0.198980	-0.056831	-0.000001	-0.056831	-0.000001	-0.000001	-0.000001	3.904398	
		-0.254255	0.072640	-0.024071				0.071782	-0.994791		-0.994791					
4		68.356659	1.007667	1.040731	0.877729	0.123479	0.074255	0.968229	0.083837	0.069147	0.083837	0.069147	0.069147	0.069147	0.069147	
		45.575607	0.250446	1.083121	0.877729	0.123479	0.074255	0.240644	-0.056225	-0.000009	-0.056225	-0.000009	-0.000009	-0.000009	4.075283	
		-0.409189	0.070769	-0.083121				0.067999	-0.994892		-0.994892					
5		66.445786	1.015993	1.054566	0.877729	0.123479	0.074255	0.963423	0.074213	0.072791	0.074213	0.072791	0.072791	0.072791	0.072791	
		45.575822	0.276570	1.112111	0.877729	0.123479	0.074255	0.261466	-0.048593	-0.000008	-0.048593	-0.000008	-0.000008	-0.000008	4.295460	
		-0.560674	0.062258	-0.112111				0.059037	-0.996053		-0.996053					
6		64.446930	1.019288	1.061253	0.877729	0.123479	0.074255	0.960458	0.056176	0.077079	0.056176	0.077079	0.077079	0.077079	0.077079	
		45.576233	0.291549	1.126257	0.877729	0.123479	0.074255	0.274721	-0.034442	-0.000008	-0.034442	-0.000008	-0.000008	-0.000008	4.446280	
		-0.691620	0.048760	-0.126257				0.045286	-0.997806		-0.997806					
7		62.353668	1.014891	1.063209	0.877729	0.123479	0.074255	0.956354	0.030596	0.083271	0.030596	0.083271	0.083271	0.083271	0.083271	
		45.576559	0.309468	1.130605	0.877729	0.123479	0.074255	0.291045	-0.011011	-0.000008	-0.011011	-0.000008	-0.000008	-0.000008	4.650612	
		-0.782579	0.027728	-0.130605				0.026078	-0.999471		-0.999471					
8		60.159760	1.002567	1.057408	0.877729	0.123479	0.074255	0.948136	0.003904	0.093574	0.003904	0.093574	0.093574	0.093574	0.093574	
		45.576935	0.336100	1.118113	0.877729	0.123479	0.074255	0.317853	0.020943	-0.000009	0.020943	-0.000009	-0.000009	-0.000009	4.874245	
		-0.810978	0.003134	-0.118113				0.002964	-0.999773		-0.999773					
9		57.856781	0.980020	1.046042	0.877729	0.123479	0.074255	0.936384	0.033193	0.104566	0.033193	0.104566	0.104566	0.104566	0.104566	
		45.577118	0.365453	1.04204	0.877729	0.123479	0.074255	0.349347	0.049444	-0.000009	0.049444	-0.000009	-0.000009	-0.000009	5.129755	
		-0.767348	-0.014466	-0.094204				-0.013832	-0.008224		-0.008224					
10		55.437408	0.93159	1.017714	0.877729	0.123479	0.074255	0.917900	0.068656	0.121867	0.068656	0.121867	0.121867	0.121867	0.121867	
		45.577118	0.402743	1.035740	0.877729	0.123479	0.074255	0.365733	0.085777	-0.000017	0.085777	-0.000017	-0.000017	-0.000017	5.410012	
		-0.642507	-0.026753	-0.035740				-0.029236	-0.993946		-0.993946					
11		53.553650	0.880072	0.974188	0.877729	0.123479	0.074255	0.903390	0.133772	0.138242	0.133772	0.138242	0.138242	0.138242	0.138242	
		45.576843	0.415318	0.949043	0.877729	0.123479	0.074255	0.426322	0.134293	-0.000018	0.134293	-0.000018	-0.000018	-0.000018	5.69014	
		-0.482450	-0.045038	0.050957				-0.046232	-0.984389		-0.984389					

PROG. J14
CASE NO. NACA

DOUGLAS AIRCRAFT COMPANY
LONG BEACH DIVISION
FRIDAY, MAR 4, 1977

PAGE 28.

NACA SWEEP WING, 8 STRIPS, A=3.22, 30 SOURCE, 1 WAKE, 1 PL-SYM. ONE
UNIFORM ONSET FLOW = (0.989707E+00, 0.0 , 0.143106E+00)

N	M	ON - BODY POINTS			FINAL OUTPUT			SIG		
		XO YO ZO	VX VY VZ	VT VTSC CP	DCX DCY DCZ	NX NY NZ	AREA			
1	12	52.581833 45.576492 -0.352118	0.759466 0.449190 -0.041023	0.883314 0.780273 0.219757	0.859792 0.508529 -0.046443	-0.165237 0.190664 -0.967589	0.148516 -0.300019 1.467240			
13		52.091583 45.578140 -0.255223	0.600241 0.572915 0.013688	0.829834 0.688708 0.311292	0.723383 0.690355 0.016494	-0.232663 0.266078 -0.935453	0.154522 -0.900018 0.764778			
14		51.819290 45.572739 -0.177842	0.424893 0.746542 0.152311	0.872386 0.761059 0.238942	0.487046 0.855747 0.174591	-0.315534 0.358787 -0.878470	0.154482 -0.300019 0.500457			
15		51.654800 45.576706 -0.070720	0.198910 0.985132 0.957211	1.287913 1.526302 -0.926302	0.143316 0.709794 0.689677	-0.559424 0.358787 -0.535179	0.145250 -0.300013 0.548432			
16		51.654724 45.577316 0.071609	1.250483 -0.212111 1.595854	2.038502 4.155488 -3.155488	0.613432 -0.104101 0.782856	-0.563258 0.637131 0.526061	-0.037122 -0.300044 0.551732			
17		51.818466 45.573776 0.180534	1.517966 -0.514027 0.777402	1.731235 3.172797 -2.172797	0.852199 -0.288579 0.436440	-0.322756 0.366581 0.872610	-0.109570 0.300004 0.501361			
18		52.090698 45.579239 0.258813	1.426581 -0.402042 0.468071	1.554537 2.416586 -1.416586	0.917689 -0.259204 0.301130	-0.232183 0.265083 0.955853	-0.122187 0.300003 0.766466			
19		52.581192 45.577886 0.356008	1.333995 -0.275412 0.283361	1.391290 1.635680 -0.935686	0.958819 -0.167954 0.203668	-0.165991 0.191233 0.967397	-0.126188 0.300009 1.468531			
20		53.553146 45.577198 0.437198	1.235990 -0.145567 0.163950	1.255401 1.576031 -0.576031	0.984538 -0.116749 0.130596	-0.114589 0.134583 0.984255	-0.117765 0.300013 2.930748			
21		55.437012 45.577621 0.648502	1.143954 -0.113140 0.087417	1.153008 1.329426 -0.329426	0.992148 -0.098126 0.077551	-0.069199 0.385725 0.933913	-0.100742 0.300013 5.411088			
22		57.856552 45.577484 0.774903	1.095542 -0.119805 0.043203	1.102920 1.216431 -0.216431	0.993311 -0.108626 0.039171	-0.033922 0.300015 0.998191	-0.085459 0.300015 5.130910			

PROGRAM JIMA
CASE NO. NACA

DONGLAS AIRCRAFT COMPANY
LONG BEACH MAR 4, 1977

NACA SWEEP WING, 8 STRIPS, A=8.22, 30 SOURCE, 1 WAKE, 1 PL-SYM. ONE
UNIFORM ONSET FLOW = (0.999707E+00, 0.0, 0.143106E+00)

ON - BODY POINTS FINAL OUTPUT

N	M	XO YO ZO	VX VY VZ	VT VTSQ VCP	DCX DCY DCZ	NX NY NZ	SIG VN AREA
1	23	60.159780 45.577087 0.020607	1.073943 -0.127297 0.008387	1.081491 1.159622 -0.159622	0.993021 -0.117705 0.007477	-0.004972 0.021450 0.999758	-0.077039 0.000015 4.875637
24		62.354095 45.576431 0.764937	1.048848 -0.121220 -0.031832	1.055310 1.115789 -0.115789	0.992936 -0.114758 -0.030135	0.029164 -0.010253 0.999522	-0.074337 0.000015 4.652055
25		64.447810 45.575684 0.707177	1.021267 -0.107099 -0.055973	1.028617 1.058052 -0.058052	0.992854 -0.104119 -0.058304	0.055130 -0.033241 0.997526	-0.073872 0.000014 4.447557
26		66.447235 45.574905 0.570778	0.995938 -0.088356 -0.076500	1.002726 1.005459 -0.005459	0.993132 -0.107629 -0.076293	0.072235 -0.047702 0.996243	-0.074281 0.000015 4.256392
27		68.359566 45.574310 0.431690	0.972942 -0.068241 -0.084207	0.979009 0.958459 0.941541	0.993802 -0.070413 -0.086013	0.022183 -0.055688 0.995080	-0.074737 0.000007 4.075724
28		70.188034 45.573922 0.279760	0.955919 -0.052535 -0.082784	0.960934 0.923395 0.076605	0.994781 -0.054675 -0.086149	0.083066 -0.056536 0.994939	-0.072822 0.000010 3.904449
29		71.516048 45.573364 0.170908	0.942978 -0.040130 -0.075402	0.946919 0.896656 0.103344	0.995838 -0.042379 -0.080685	0.078403 -0.053293 0.995496	-0.065132 0.000012 1.987977
30		72.373566 45.572830 0.103344	0.933524 -0.027761 -0.075021	0.936945 0.877865 0.122135	0.996349 -0.029629 -0.080070	0.078404 -0.053321 0.995495	-0.064949 -0.000011 1.851551

THE FORCE COMPONENTS OF THIS STRIP ARE

THE MOMENT COMPONENTS OF THIS STRIP ARE

-0.225973E+01 0.266826E+01 0.694168E+01
0.315769E+03 -0.347150E+03 0.242923E+03

2	1	70.630321 42.094534 -0.080126	0.924951 0.935520 0.076703	0.932351 0.860279 0.120721	0.992063 0.100305 0.075832	0.081374 -0.052762 -0.995234	0.059918 -0.000037 2.513206
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6.0 ACKNOWLEDGMENT

The author is grateful to Mr. Douglas Smyth for his contributions to the modification work of the streamline calculation from the Mark IV supersonic-hypersonic arbitrary-body program. The author is also indebted to Mr. Kalle Kaups for his valuable advice and suggestions made on the modification work of the small crossflow boundary-layer program. Finally, the author would like to acknowledge the significant effort by Mrs. Sue Schimke who assisted in checking out and analyzing the programming results.

7.0 REFERENCES

1. Hess, J.L.: A Fully Automatic Combined Potential-Flow Boundary-Layer Procedure for Calculating Viscous Effects on the Lifts and Pressure Distributions of Arbitrary Three-Dimensional Configurations. Douglas Aircraft Company Report No. MDC J7491, June 1977.
2. Mack, D.P. and Schimke, S.M.: User's Manual for a Fully Automatic Combined Three-Dimensional Potential-Flow Boundary-Layer Program. Douglas Aircraft Company Report No. MDC J7644/01, 1 August 1977.
3. Gentry, A.E., Smyth, D.N. and Oliver, W.R.: The Mark IV Supersonic-Hypersonic Arbitrary-Body Program. Technical Report AFFDL-TR-73-159, Nov. 1973.
4. Cebeci, T.: Calculation of Three-Dimensional Boundary Layers. I. Swept Infinite Cylinders and Small Cross Flows. AIAA J., Vol. 12, No. 6, June 1974. (Also McDonnell Douglas Report No. MDC-J5694, Nov. 1972.)

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Computer Program	Potential Flow	Vorticity												
Input-Output	Pressure Distribution	Wing-Body												
Kutta Condition	Three-Dimensional Flow													
20. ABSTRACT (Continue on reverse side if necessary and identify by block number)														
<p>This report describes a computer program which calculates three-dimensional viscous effects on the lift and pressure distributions of arbitrary three-dimensional bodies. The program is a combination of a panel method, which computes the potential flow about arbitrary three-dimensional lifting configurations, and a three-dimensional boundary-layer method, which calculates the viscous effects with small crossflow. These effects are applied to the three-dimensional shape, as in Part 1, in a "strip-theory" sense and the resultant</p>														

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
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20. Abstract (cont.)

viscous lift and pressure distributions are again produced. The method of simulating the boundary layer in the final potential-flow calculation is by the addition of the displacement thickness to the original shape.

The computer program is written in Fortran IV for the IBM 370 systems. 16 temporary external units are used for storage. The region size needed to execute the program is about 360K bytes, but this is a direct function of the number of elements defining the configuration. 

Also presented in this report is a detailed description of the program logic, complete instructions for executing the program, and a sample case. The basic description of the method, its background and capabilities is contained in McDonnell Douglas Report MDC J7491, "A Fully Automatic Combined Potential-Flow Boundary-Layer Procedure for Calculating Viscous Effects on the Lifts and Pressure Distributions of Arbitrary Three-Dimensional Configurations" by John L. Hess.

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